

THE EFFECT OF SILANE COUPLING AGENT ON IRON SAND FOR USE IN MAGNETORHEOLOGICAL ELASTOMERS

PART 1: SURFACE CHEMICAL MODIFICATION AND CHARACTERIZATION

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ABSTRACT

Bis-(3-triethoxysilylpropyl) tetrasulphane (TESPT) was employed for surface modification of iron sand for use in magnetorheological elastomers (MREs). The amount of TESPT was varied at five levels (2,4,6,8 and 10wt%) relative to iron sand content to assess the optimum amount of coupling agent for interfacial bonding and damping performance. Evidence that coupling had occurred between iron sand and TESPT was identified by Raman Spectroscopy and the grafting percentage was determined by thermogravimetric analysis. Subsequently, isotropic MREs containing unmodified and modified iron sand particles and natural rubber were prepared. Crosslink density assessment by swelling testing provided evidence that the tetrasulphane group of TESPT formed crosslinks with the rubber chains. The results exhibited the advantages of TESPT as a coupling agent between iron sand particles and rubber and also revealed that 6% TESPT content produced the highest crosslink density. The effects of the amount of TESPT on dynamic mechanical properties the morphological characteristics of the MREs were also investigated.

Keywords: A. Particle-reinforcement; B. Interface/interphase; D. Surface analysis; E. Surface treatments

INTRODUCTION

Magnetorheological elastomers (MREs) are a new group of damping materials which consist of a non-magnetic matrix (normally an elastomer) containing a suspension of magnetically permeable particles. The most commonly used magnetic particles for MREs are carbonyl iron particles and suitable matrix materials include natural rubber, silicone rubber, polybutadiene, polyisobutylene, polyisoprene, and polyurethane rubber [1-7]. The main advantage of MREs is that the damping and stiffness can be varied by application of an applied magnetic field during fabrication or in service. Damping occurs by the viscous flow of the rubber matrix and inclusion of magnetic particles in rubber enables additional damping through magnetic particle interaction and interfacial damping. MREs can be classified into two kinds: isotropic MREs and anisotropic MREs. Isotropic MREs can be characterized by having a uniform magnetic particle distribution in the matrix. Anisotropic MREs have a special chain-like structure of magnetic particles in a matrix resulting from curing the matrix under an applied magnetic field. Over the past few years, MREs have attracted increasing attention and have been considered for applications such as adaptive tuned vibration absorbers [8], automotive engine mounts [4] and semi active seismic dampers [9].

New Zealand iron sand possesses physical and magnetic properties that make it suitable for use in MREs. Compared to commonly use magnetic particles, such as pure iron and carbonyl iron, iron sand has a number of advantages, including high permeability and saturation magnetisation, low cost and it is readily available in New Zealand. It is derived from erosion of andesitic and rhyolitic volcanic rocks which are the main types of iron ore deposits in New Zealand. Iron sand is a dark, high-density sand that occurs along the west coast of the North Island from Wanganui to Kaipara Harbour near Auckland, over a distance of 480 km. It contains titanomagnetite, a mineral containing iron and titanium, which is highly magnetic [19, 20].

Similarly for all MREs, the damping of MREs depends not only on the types of rubber matrix and magnetic particles, but also on the level of adhesion between the particles and the rubber matrix such that the strength of interaction between the particles and matrix has to be sufficiently strong to obtain efficient interfacial damping. For MREs this sets a challenge. Here, as for other MRE components, the incompatibility of the inorganic magnetic fillers and the matrix can actually lead to poor wettability and adhesion between the filler and matrix as well as non-uniformity of filler dispersion leading to low energy absorption [10-12]. Therefore, it is sensible to modify the surface of the iron sand in order to improve ease of adhesion with and dispersion within the rubber matrix in order to realise the full potential of MREs.

Surface modification of inorganic particles can be achieved using a number of approaches [13]; most commonly, the filler surface is chemically modified to become more compatible with the matrix using methods such as polymer coating [14], surfactant absorption [15] and bifunctional coupling agent treatments [16, 17]. Among various modification approaches, the bifunctional coupling agent treatment using silane based coupling agents is the most successful and cost effective treatment for improving the adhesion between inorganic particle and rubber matrix. These chemicals are silicon-based chemicals that contain hydrolysable groups (such as methoxy, ethoxy or acetoxy) at one end that will interact with inorganic materials and organofunctional groups (such as amino, vinyl or sulphide) at the other end that can react with the rubber matrix. Therefore, inorganic and organic materials can be coupled together with the silane coupling agent acting as a bridge between them. Although this type of surface modification is well established for enabling different types of fillers such as silica [18, 19], aluminium powder [20], halloysite nanotubes [21], wood flour [22] and natural fibre [23, 24] to be used as reinforcement fillers in rubber compounds, its effect on inorganic magnetic particles for used in MREs has not been

extensively studied. Some research has been reported on modification of carbonyl iron particles using silane coupling agents used as a filler in silicon rubber [25, 26] and polyurethane rubber [16] based MREs; the results showed that the mechanical and damping performance of MREs increased due to increased dispersion and interaction between particles and the matrix. Although it is accepted that the effectiveness of silane to interact with the substrate is dependent on a number of factors including hydrolysis time, presence of solvent, temperature and pH [27], none have assessed the optimum silane content coupled to the particles to allow for improved subsequent bonding. Furthermore, as far as the authors are aware, there is no work carried out on surface modification of inorganic magnetic particles for use in natural rubber based MREs.

In this study, isotropic MREs based on iron sand and natural rubber were prepared. Bis-(3-triethoxysilylpropyl) tetrasulphane (known as TESPT or Si 69) which is the most popular and effective silane coupling agent for hydrocarbon rubber (see Figure 1) was used for surface modification of iron sand particles [13]. TESPT contains ethoxy hydrolysable groups at both ends that enable the silicon groups to bond with iron sand particles and the tetrasulphane group of its centre which is capable of bonding with the rubber matrix. Iron sand contains stable oxides that potentially have reactive sites including Fe-O bonds and OH groups on their surface [28, 29]. Therefore, there is potential for improvement of iron sand and natural rubber interaction by using TESPT as a coupling agent. The effects of TESPT content on dynamic mechanical properties were investigated using two methods. The loss tangent, commonly called $\tan \delta$, is considered as the fundamental parameter to assess damping. $\tan \delta$ gives a comparison of the energy lost to that stored; it is obtained by dividing the loss modulus (G'' or E'') by the storage modulus (G' or E') [30]. The other estimate of damping used was the amount of energy dissipated during cyclic deformation, which can be calculated from the area of the hysteresis loop (hysteresis loss).

EXPERIMENTAL

Materials

Natural rubber (SMR L grade) and other chemicals including zinc oxide, stearic acid, n-cyclohexyl-2-benzothiazole sulfenamide (CBS), tetramethylthiuram disulphide (TMTD), paraffin oil, and naphthenic oil were all purchased from Field Rubber Limited, Auckland. Bis-(3-triethoxysilylpropyl) tetrasulphane (TESPT) was purchased from Leap LabChem Co. Limited, China. Iron sand was collected from Ngarunui Beach, Raglan. The iron sand was milled using a planetary mono mill (Pulverisette 6) produced by Fristech GmbH and subsequently sieved to obtain a 45-56 μm particle size.

Surface Modification of Iron Sand Particles

The surface modification of iron sand particles was carried out by an aqueous alcohol solution method. The particles were subjected to surface treatment with TESPT at 2, 4, 6, 8, 10% by weight (wt%) of the particles. An aqueous alcohol solution of 95% ethanol was used and the pH of the solution was adjusted with acetic acid to 4.0 – 4.5. The TESPT of predetermined quantity was dispersed in the ethanol solution at a ratio of 1:100 and the mixed solution was stirred for 5 minutes to assure the hydrolization of the silane coupling agent. The iron sand particles were then added and stirred for an additional 30 minutes at room temperature to ensure a uniform distribution of the coupling agent on the surface of iron sand particles. The mixture was filtered and washed three times with ethanol to remove unreacted coupling agent. The treated iron sand particles were then dried at 80°C in an oven until a constant weight was achieved.

Preparation of iron sand-natural rubber isotropic MREs

The compound formulation used in this study is given in Table 1. Formulations were compounded using a conventional laboratory two roll mill (model XK150) according to ASTM designation D3184-80. The front roller speed was 23.86 rpm and the rear roller speed was 32.81 rpm, diameter of rolls was 150 mm, friction ratio of two rolls was 1:1.4 and the roller temperature was set at 80°C. The nip gap (distance between front and back roller) was maintained at 2 mm during compounding. The compounding began with softening the rubber on its own in the two roll mill (mastication). Mastication reduces the viscosity and increase the plasticity of natural rubber which is brought about by heat generated in two roll mill through conduction from the heated roller and shearing of rubber during milling. After mastication, during which the rubber had become invested on the hot roll (2-3 minutes), additives (other than accelerators and sulphur) were then added followed by iron sand; addition of accelerators and sulphur were delayed to the last part of the process to prevent premature vulcanization during compounding. The mixing time was approximately 40 minutes. The cure time at 150°C was then determined according to the procedure as described in reference [31] and the results are shown in Table 1. Compounded rubber samples weighing 13g were placed in a mould 60 x 50 x 3 mm and were cured in a compression moulder at 150°C under a pressure of approximately 12 MPa

Raman spectroscopy

Raman spectra were acquired with a Ramanstation 400R (PerkinElmer) spectrometer equipped with an air cooled charged coupled device (CCD) detector and data points were recorded at 1 cm⁻¹ intervals. The excitation source was a 785 nm near infrared laser focused on surface of samples with a spot approximately 200 µm in diameter. Calibration was validated against a polystyrene standard disk (PerkinElmer) prior to measurement. Samples were analysed while placed on aluminium foil. The Raman instrument was visually focused onto the surface of each

location to be analysed on the modified iron sand samples. Laser power was set to approximately 40mW (40% of maximum, estimated to be $6 \times 10^5 \text{ W/m}^2$ on the 200 μm diameter spot) to acquire spectra from all samples (after initial trials) for consistency across the range of materials analysed. Spectra were collected over the range 3200 – 200 cm^{-1} and each spectrum was acquired as the sum of five repeats of 60s exposures on the sample. Five separate spectra were acquired at different locations on each sample analysed.

Thermogravimetric analysis

The grafting percentage of silane coupling agent with iron sand particles was determined by thermogravimetric analysis (TGA) using an TA Instrument SDT 2910 thermal analyser operated in dynamic mode, heating from ambient temperature to 300°C at 5°C/min in air purged at 150 ml/min with an empty pan used as a reference. Thermal gravimetric curves were obtained. The grafting percentage was calculated as the fraction of the mass of grafted silane coupling agent divided by the mass of iron sand particles at 280°C [32, 33] as follows:

$$\text{Silane grafting (\%)} = \frac{\text{Grafted silane coupling agent/g}}{\text{iron sand particles/g}} \quad (1)$$

The amount of grafted silane coupling agent was calculated from the weight loss of treated iron sand at 280°C minus weight loss of iron sand particles at 280°C.

Crosslink Density

Determination of crosslink density in MREs was obtained using a swelling test. MREs samples with dimensions of 30mm \times 5mm \times 3 mm were weighed, and then immersed in toluene for 72 hours at room temperature in a dark environment. The toluene was replaced at 24 hours intervals over this time to minimise interference from toluene soluble fractions remaining in the samples. After 72 hours, samples were drained and dried and the swollen mass was recorded. Samples were then dried at 80°C in an oven until a constant weight was achieved. For each experimental point,

3 samples were produced and the average values were calculated. The crosslink density was calculated by applying the Flory-Rehner equations as follows [34]

$$V_r = \frac{V_p}{V_p + V_s} = \frac{\frac{m_{dry}}{\rho_r}}{(\frac{m_{dry}}{\rho_r} + \frac{m_{wet} - m_{dry}}{\rho_s})} \quad (2)$$

$$[X] = \frac{-[\ln(1 - V_r) + V_r + \chi V_r^2]}{V_o (V_r^{\frac{1}{3}} - \frac{V_r}{2})} \quad (3)$$

where V_r is the volume fraction of MREs, m_{wet} is the swollen equilibrium mass, m_{dry} is the dry MREs mass, ρ_r is the density of natural rubber (910 kg/m³), ρ_s is the density of toluene (866 kg/m³), $[X]$ represents the crosslink concentration in mol/cm³, χ is the interaction parameter between the rubber and toluene (0.393) and V_o is the molar volume of toluene (106.4 cm³/mol).

Morphology

The microstructures of isotropic MREs were observed using a Hitachi S-4700 scanning electron microscope (SEM). The samples were frozen and snapped into pieces to expose their interior and coated with a thin layer of platinum prior to observation at an accelerating voltage of 20kV.

Dynamic mechanical analysis

Dynamic mechanical analysis was carried out using a Perkin Elmer dynamic mechanical analyser (DMA 8000). $\tan \delta$ was measured over a wide range of frequency, strain amplitude and temperature. The influence of frequency and strain amplitude on $\tan \delta$ was assessed using two circular disc specimens with a diameter of 10mm and a thickness of 3mm in shear mode at room temperature. $\tan \delta$ was measured over the frequency range of 0.01–130 Hz at a fixed strain amplitude of 0.5% and over a strain amplitude range of 0.1–4.5% at a fixed frequency of 100Hz. For the influence of temperature on $\tan \delta$, the samples were analysed in dual cantilever mode at a

frequency of 1 Hz, with a strain amplitude of 0.5% over a temperature range of -100 – 50 °C. The samples were rectangular with dimensions 30 mm × 6 mm × 3 mm.

Hysteresis

Hysteresis loss is defined as the amount of energy dissipated during cyclic deformation when the samples are stretched and then allowed to retract at the same rate to the unstretched state. In this study, the hysteresis loss was determined for tensile dumbbells using an Instron 4204 at a crosshead speed of 500mm/min according to ASTM D412-80. The stress-strain curve was recorded and hysteresis loss was calculated as

$$\text{Hysteresis loss} = \text{Area under the loading curve} - \text{Area under the recovery curve} \quad (4)$$

RESULTS AND DISCUSSION

Characterization of surface modified iron sand particles

Figure 2 shows a schematic of the potential reaction mechanisms of TESPT with iron sand particles. In the presence of water in an ethanol solution and under acid catalysed conditions the ethoxy reactive groups of the silane are hydrolysed thereby forming silanol groups (-Si-O-OH) and liberating ethanol [35, 36]. The silanol groups are highly reactive intermediates which are presumed responsible for bond formation with the iron sand. When iron sand was added into the solution, the hydroxyl groups on the surface of the iron sand is believed to react with the silanol groups and subsequent drying condenses silanol groups to form siloxane linkages. Evidence for this was provided by Raman Spectroscopy analysis of unmodified and modified iron sand particles as shown in Figure 3. For iron sand, a number of peaks can be seen including a broad peak between 1100 and 1900 cm^{-1} , similar to observation elsewhere [37]. The growth of peaks at around 300 cm^{-1} for all modified iron sand particles is indicative of the formation of Si-O-iron sand and/or Si-O-

Si bonds that would occur during reaction of iron sand with TESPT, although, the latter could also occur due to polymerisation of TESPT to produce siloxane; however, production of siloxane would not be expected to improve interfacial bonding. The increased height of the peaks around 1400 cm^{-1} (representing CH_2 bending in TESPT) from 0 to 6 wt% TESPT followed by no further increase from 6 wt% onwards suggests that coverage of iron sand particles by TESPT increases to 6 wt% when it reaches a saturation coverage [38].

Figure 4 shows TGA curves for unmodified and modified iron sand particles at different TESPT contents. All samples showed weight loss over the temperature range of 50°C to 280°C with weight increase above 280°C which is believed to have resulted from the oxidation of iron sand particles [39]. Similar trends have been observed in TGA curves for other magnetite particles [40]. As can also be seen, the unmodified iron sand particles were relatively stable in the air and only slightly weight loss between 100°C to 280°C which was probably due to vaporization of physically absorbed water at the surface of iron sand particles. The weight losses for modified particles increased with increasing TESPT content until 6% and then reduced for 8% and 10% TESPT. The weight loss for modified particles could be attributed to the decomposition and evaporation of silane coupling agent on the surface of iron sand particles such that suggests the silane coupling agent is strongly bound to particle surfaces by what is expected to be covalent bonds [41]. The amount of TESPT attached to the surfaces of iron sand particles was quantitatively determined by TGA (taking the loss due to physically absorbed water into account) over the temperature range of 50°C to 280°C (each value representing an average from 3 samples) and is presented in Figure 5. It was not possible to conduct TGA analysis of TESPT on its own, however, a separate experiment was conducted where TESPT was heated at 280°C in a furnace for which a residual weight of only 0.6% was obtained. Thus, residual TESPT is not considered to have a

significant effect on the obtained data. It can be seen that the percentage of grafted silane appears to increase with increasing TESPT content until it reached a maximum value at 6% TESPT and thereafter decreased for higher TESPT contents (8% and 10%). At high TESPT content, the potential for hydrolysed TESPT to react with itself to produce polymeric siloxane increases as an alternative to reacting with iron sand. This polymeric siloxane could act as a barrier between TESPT and iron sand preventing reaction, particularly given that the siloxane polymer can react with multiple OH groups on the iron sand particles and screen other OH groups between those bonded with polymeric siloxane as described in the literature [42]. Polymeric siloxane that has not reacted with OH groups on iron sand would easily have been removed by washing the modified iron sand with ethanol and evaporation by drying during the preparation of the modified particles. This was checked by an extra wash with dichloromethane (DCM) following three times washing with ethanol for which the TGA weight loss and silane grafting percentage was found to be no significant different with those washed using just ethanol. Any remaining unreacted polymeric siloxane may also form e.g. oligomers by hydrogen bonding to the grafted TESPT such that may weaken the composites properties since the silane molecules may not link the filler to the matrix [42].

Figure 6 shows a schematic of possible reaction mechanisms for the tetrasulphane group of TESPT with natural rubber. The tetrasulphane group of the TESPT could have been first dissociated during the compounding process to produce sulfidic radicals that subsequently react either directly or through sulphur crosslinking agent (S_x) with the rubber molecules in the presence of accelerators at elevated temperature during vulcanization to form crosslinks with the rubber molecules [43-45]. Evidence for this would be provided by crosslink density measurements of MREs filled with unmodified and modified iron sand particles at different TESPT contents as

shown in Figure 7. It can be seen that the crosslink density gradually increased as the TESPT content increased from 2% to 6%; this highlights the potential formation of new crosslinks in the rubber network due to interaction between tetrasulphane group of TESPT with the rubber molecules. In order to assess the time required for the tetrasulphane group of TESPT to react with rubber and form crosslinks, another compound was prepared, the same as that containing 6 wt% silane coupling agent except that the sulphur crosslinking agent was excluded. It was found that the compound cured in 5.63 minutes which is not too different from time used here supporting substantial TESPT rubber crosslinking could have occurred. At higher TESPT contents (8% and 10%) the crosslink density decreased which is not surprising given the evidence from TGA results that at such TESPT contents less silane is coupled to the iron sand, which would be expected to lead to less crosslinking between iron sand and rubber. The obtained results support the use of TESPT as a coupling agent for iron sand particles and natural rubber and also a content of 6% TESPT is more suitable than 8% and 10% TESPT.

Morphology

Figure 8 shows SEM images of fracture surface of isotropic MREs with unmodified and modified iron sand particles. It can be seen for unmodified particle MREs, the surface is smooth with less matrix tearing and uneven distribution of iron sand particles in the rubber matrix. Clearly, there are a lot of cavities remaining due to the particle pull out from the rubber matrix and obvious gaps between iron sand particle and rubber, suggesting weak interaction between iron sand and rubber (Figure 8 a). In Figure 8 b, the surface of isotropic MREs with modified iron sand particles is rougher due to matrix tearing than for MREs with unmodified particles. It is also evident that iron sand particles are more evenly dispersed in the rubber with much less aggregates in the matrix.

Clearly, much less particle pullout can be seen supporting improved interfacial adhesion between iron sand and natural rubber suggesting stronger interaction between iron sand and rubber was obtained by using modified iron sand particles supporting Si-O-iron sand bonding.

Dynamic Mechanical Properties

The variation of $\tan \delta$ with frequency for MREs with different TESPT contents is shown in Figure 9a. $\tan \delta$ is the highest for the MREs with modified iron sand treated with 6% TESPT and the increases in $\tan \delta$ compared to MREs with unmodified iron sand is on average 40% over the whole frequency range explored. G' and G'' are also plotted in Figure 9 (b and c) to help highlight the mechanisms involved. G' and G'' , similar to $\tan \delta$ are frequency dependent. It can be seen that the increase of $\tan \delta$ as the frequency increased, is mainly due to increasing G'' as opposed to changes in G' . The increased energy loss is assumed to be due to covalent bonding bringing about more intimate contact between the particles and rubber such that during deformation, increasing energy is expended overcoming friction, physical bonding as well as covalent bonding. At high TESPT content (8% and 10%), the lower $\tan \delta$ values could again be explained by less silane grafting due to the formation of siloxane oligomer attached to the first layer of reacted TESPT on particle surfaces which could further reduce the energy absorption capability of the MREs. Energy loss in the materials could also be attributed to interfacial friction of weakly or partially bonded iron sand particles and rubber with increasing frequency. It is also apparent that the G' for MREs with modified iron sand are higher compared to MREs with unmodified iron sand. Explanation for general increment of G' for MREs with modified iron sand could be related to efficient stress transfer between particles and matrix which can improve stiffness, strength and failure strain of the materials [46]. Furthermore, improved interfacial

bonding and degree of iron sand particle dispersion in the matrix might increase the effective particle-matrix interfacial area such that increased constraint of polymer chains occurs during deformation and improved the ability of the material to store elastic energy associated with recoverable elastic deformation [47].

The variation of $\tan \delta$ with strain amplitude for MREs with different TESPT contents is shown in Figure 10a; G' and G'' are also plotted in Figure 10 (b and c). As expected, MREs with modified iron sand treated with 6% TESPT had the highest $\tan \delta$ over the whole strain amplitude range explored with a 20% increase in $\tan \delta$ compared to MREs with unmodified iron sand. As can be observed in Figure 10 (a and b), the $\tan \delta$ and G' were amplitude dependent at low strain amplitudes before reaching a plateau, with the $\tan \delta$ for MREs with modified iron sand reaching a plateau at around 2.5% strain amplitude, whereas the $\tan \delta$ of the MREs with unmodified iron sand reached a plateau at 2% strain amplitude. It was evident that strong interfacial bonding between the iron sand and rubber as well as better dispersion increased the dependency of $\tan \delta$ on the amplitude of the applied strain and the change of $\tan \delta$ values over the strain amplitude range for all tested samples is mainly due to a decrease in G' as the strain amplitude increased. The decrease in G' as the strain amplitude increased for MREs with modified iron sand could be explained by the increase of particle detachment from the matrix with increasing strain amplitude. As can also be seen, G'' for MREs with modified iron sand are higher compared to MREs with unmodified iron sand. The higher loss modulus could be attributed to the energy loss due to stress released after debonding and increase of energy absorbed during viscous flow which is more constrained due to formation of chemical linkages between iron sand and rubber. Once the strain amplitude is high enough, all the interactions are destroyed to such an extent it cannot be reconstructed and consequently, the energy loss is largely reliant on the viscous flow of the rubber matrix.

Figure 11 presents the $\tan \delta$ versus temperature curves for MREs with different TESPT contents. The $\tan \delta$ peak is associated with glass transition temperature (T_g) of the materials. In the glass transition zone, the energy dissipation is mainly from the segmental motion of macromolecular chain of rubber matrix in spite of breakdown of filler-filler or filler rubber interaction [48]. It can be seen that the presence of coupling agent does not strongly affect the peak height and width of the curves. This is in agreement with similar finding reported by other researchers [23, 49, 50]. However, an enlarged graph of the $\tan \delta$ versus temperature around the peaks showed a slight decrease of the height of the $\tan \delta$ peak and the T_g values shifted to a slightly higher temperature for MREs with modified iron sand compared with MREs with unmodified iron sand. In addition, the decreased height of the $\tan \delta$ peak was in an order similar to the silane grafting percentage as previously discussed. The decrease height of the damping peak and a shift of T_g to higher temperature could be attributed to strong filler rubber interaction which resulted in restriction in mobility and flexibility of rubber chains in the materials.

Figure 12 shows hysteresis loss for MREs with different TESPT contents. As can be seen, hysteresis loss increased with increasing TESPT content until it reached a maximum value at 6% TESPT and thereafter decreased at higher TESPT content (8% and 10%). The results are in agreement with the silane grafting percentage as previously discussed. The effect of coupling agent on the hysteresis loss of MREs could again be explained by the energy loss due to stress released after debonding and increase of energy absorbed during viscous flow which is more constrained due to formation of chemical linkages between iron sand and rubber. Some authors have considered constraint in liaison of a rubber shell mechanisms [13]. The molecular chain mobility would be reduced by the formation of silane linkages between iron sand and rubber, resulting in a rubber shell on the filler surface in which the polymer viscosity and Young modulus would be

increased. The higher Young's modulus of rubber near the surface of iron sand in the rubber shell would gradually decrease with increased distance from the filler surface and finally reach the same level as that of the rubber matrix at a certain distance. When the MREs were subjected to dynamic strain, the rubber shell around the particles would begin to break down and increase the amount of energy loss. In addition, hysteresis loss could also be attributed to interfacial friction at the filler matrix interface and breakdown of filler aggregates. The decrease of hysteresis loss at higher TESPT content could again be explained by the lower silane grafting and formation of weak siloxane oligomer that may begin to break down at a relatively lower level of strain.

CONCLUSION

In this work, iron sand particles were modified at five different TESPT contents (2, 4, 6, 8 and 10 wt%) relative to the iron sand content to assess the optimum amount of for use in MREs. TESPT contains ethoxy hydrolysable groups that enable bonding with iron sand particles and a tetrasulphane group capable of bonding with the rubber matrix. Raman spectroscopy showed evidence that siloxane linkages were formed between TESPT and iron sand. Weight loss measured using TGA supports that silane coupling agent is strongly bound to particle surfaces and the silane grafting percentage was found to be the highest at 6% TESPT. Crosslink density measurement of MREs made using TESPT treated iron sand highlight that the tetrasulphane group of TESPT formed crosslinks with the rubber molecular chains. Treated iron sand was found to be more evenly dispersed in the rubber with much less particle pullout on fracture surface supporting improved interfacial adhesion with natural rubber. $\tan \delta$ was found to be highest for the MREs with modified iron sand treated with 6% TESPT and 40% larger than that unmodified iron sand over the whole frequency range explored and 20% higher over the whole strain amplitude explored. However, the presence of coupling agent did not strongly affect the peak temperature of $\tan \delta$ versus temperature

curves. An increase in hysteresis loss was also obtained for MREs with modified iron sand treated with 6% TESPT content compared with MREs with unmodified iron sand.

ACKNOWLEDGEMENTS

The authors would like to thank for the support from the Polymer and Composite Research Group of the University of Waikato.

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FIGURE CAPTIONS

Figure 1 Molecular structure of TESPT

Figure 2 Illustration of the reactions of TESPT with iron sand particle surface.

Figure 3 Raman spectra of iron sand particles at different TESPT contents

Figure 4 TGA curves for iron sand particles at different TESPT contents

Figure 5 Silane grafting percentage for iron sand particles at different TESPT contents

Figure 6 Schematic illustration of the reaction mechanisms of tetrasulphane group of TESPT with the natural rubber ($S_2\bullet$ represents sulfidic radicals of tetrasulphane group of TESPT)

Figure 7 Crosslink density of MREs with different TESPT contents.

Figure 8 SEM images of fracture surface of isotropic MREs with; (a) unmodified and (b) modified iron sand particles (treated with 6% TESPT)

Figure 9 (a) $\tan \delta$, (b) storage modulus (G') and (c) loss modulus (G'') vs. frequency for MREs with different TESPT contents.

Figure 10 (a) $\tan \delta$, (b) storage modulus (G') and (c) loss modulus (G'') vs. strain amplitude for MREs with different TESPT contents.

Figure 11 $\tan \delta$ versus temperature curves for MREs with different TESPT contents.

Figure 12 Hysteresis loss for MREs with different TESPT contents.

TABLE CAPTION

Table 1 Formulation of rubber compound

		Table 1					
Materials	Function	loading (phr)					
natural rubber	raw material/matrix	100	100	100	100	100	100
ZnO	activator/peptiser	5	5	5	5	5	5
stearic acid	activator/peptiser	1	1	1	1	1	1
paraffin oil	plasticiser	2	2	2	2	2	2
naphthenic oil	plasticiser	3	3	3	3	3	3
iron sand	filler	70	70	70	70	70	70
CBS	accelerator	2	2	2	2	2	2
TMTD	accelerator	1	1	1	1	1	1

sulphur	crosslinking agent	1.5	1.5	1.5	1.5	1.5	1.5
Silane coupling agent level (wt %)							
TESPT	coupling agent	0	2	4	6	8	10
Curing characteristics (minutes)							
Cure time	(t ₉₀)	4.57	4.53	4.33	4.23	4.40	4.46

* phr = per hundred rubber

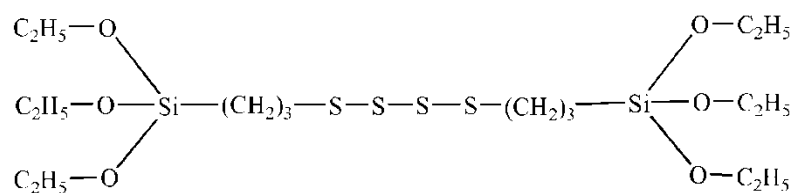


Figure 1

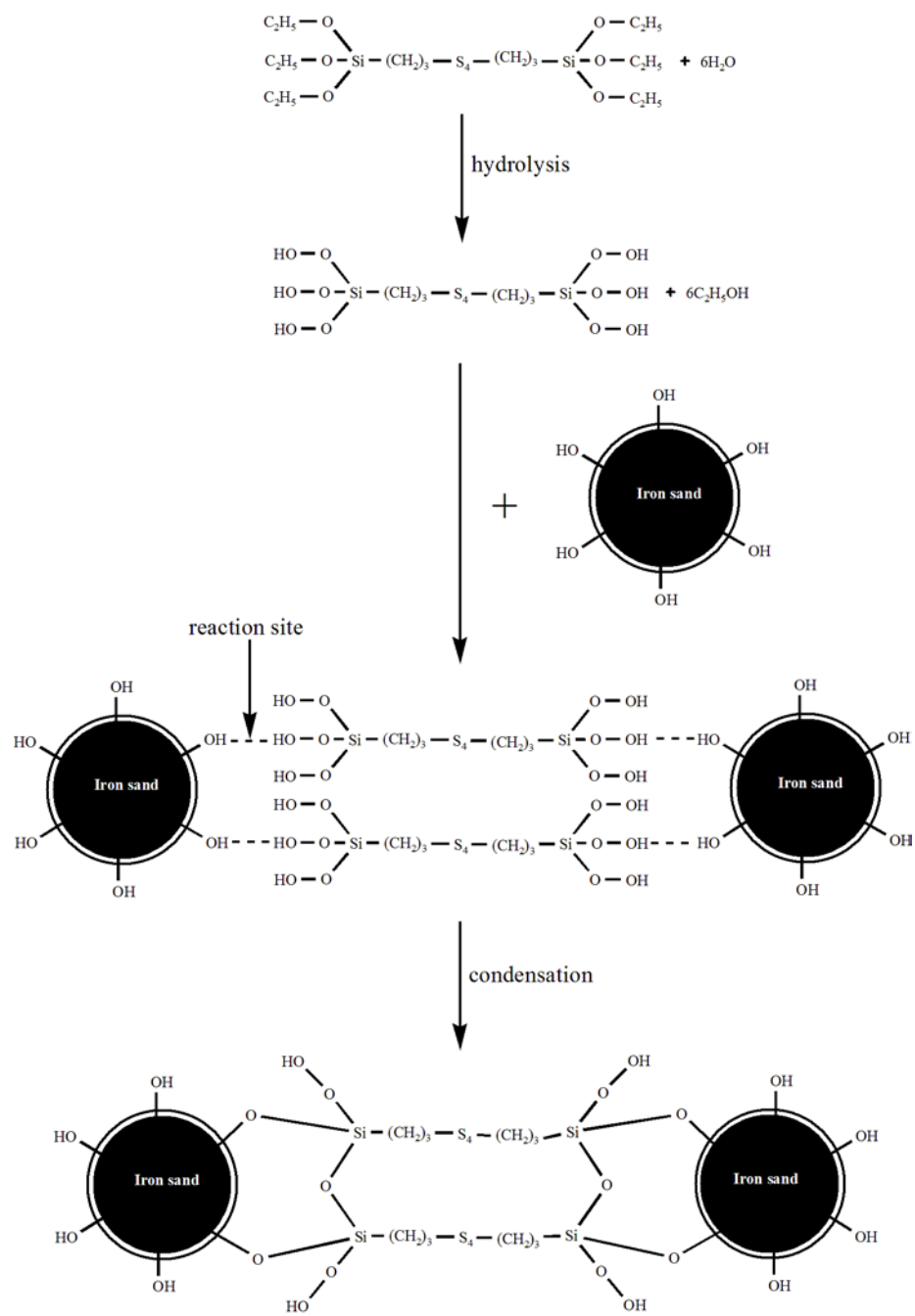


Figure 2

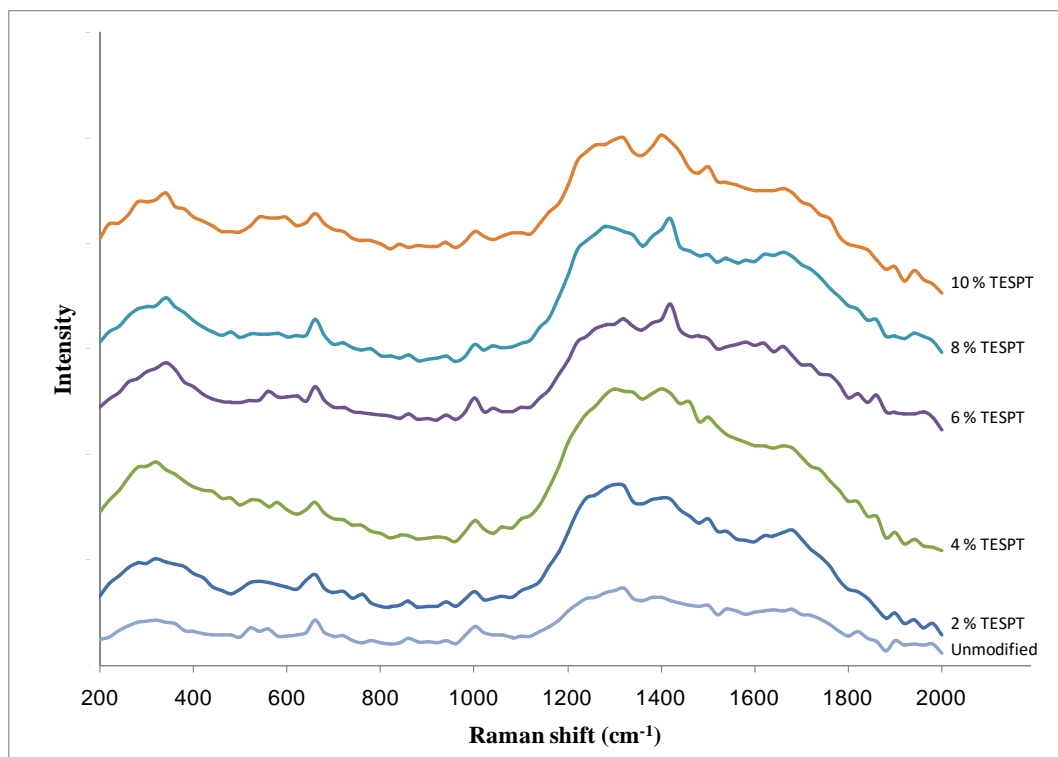


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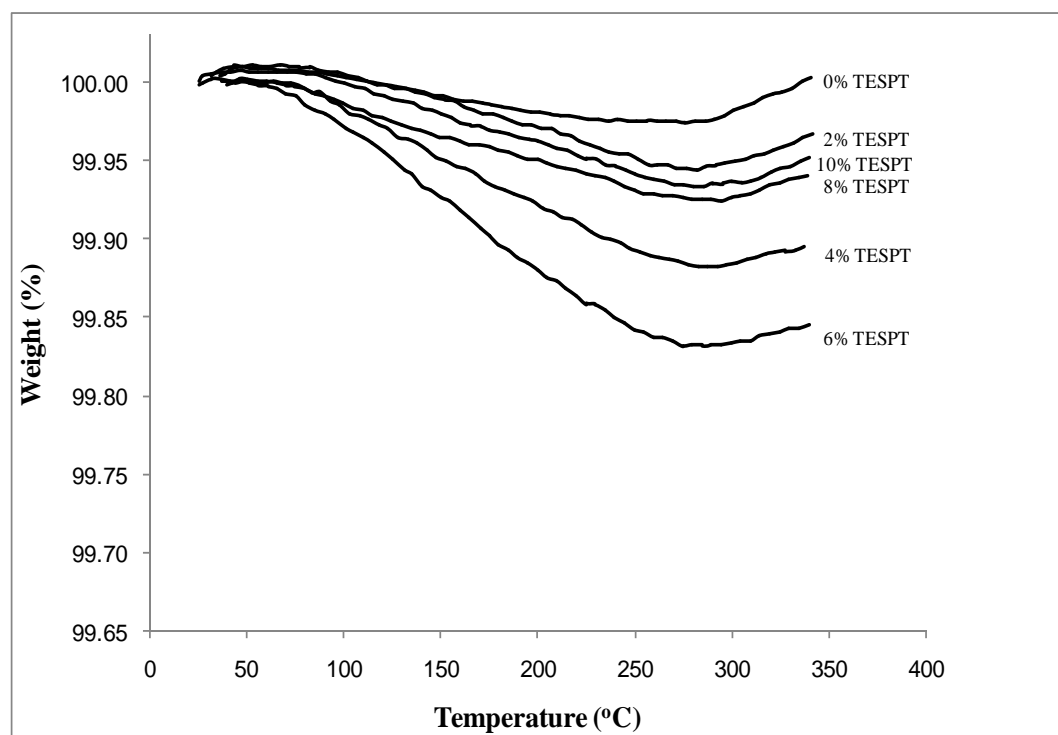


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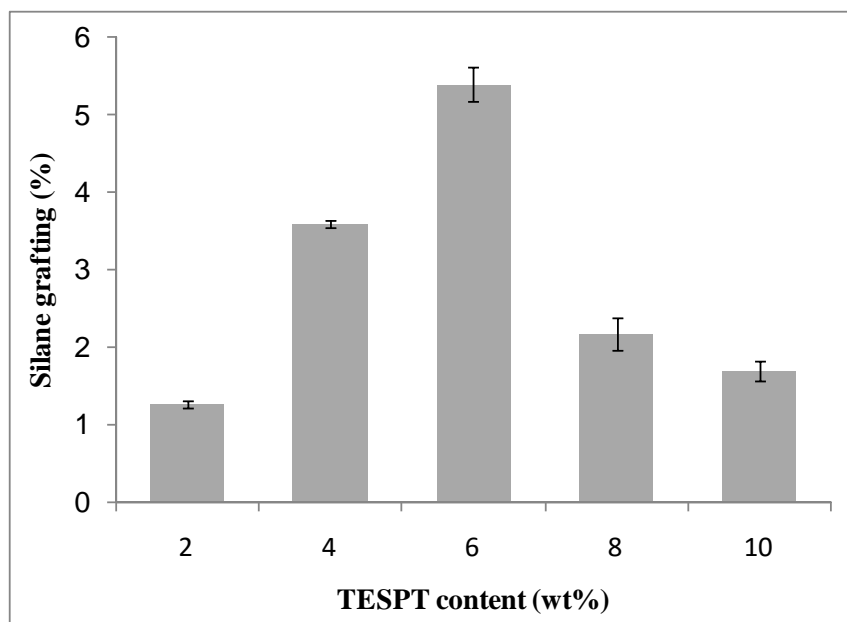


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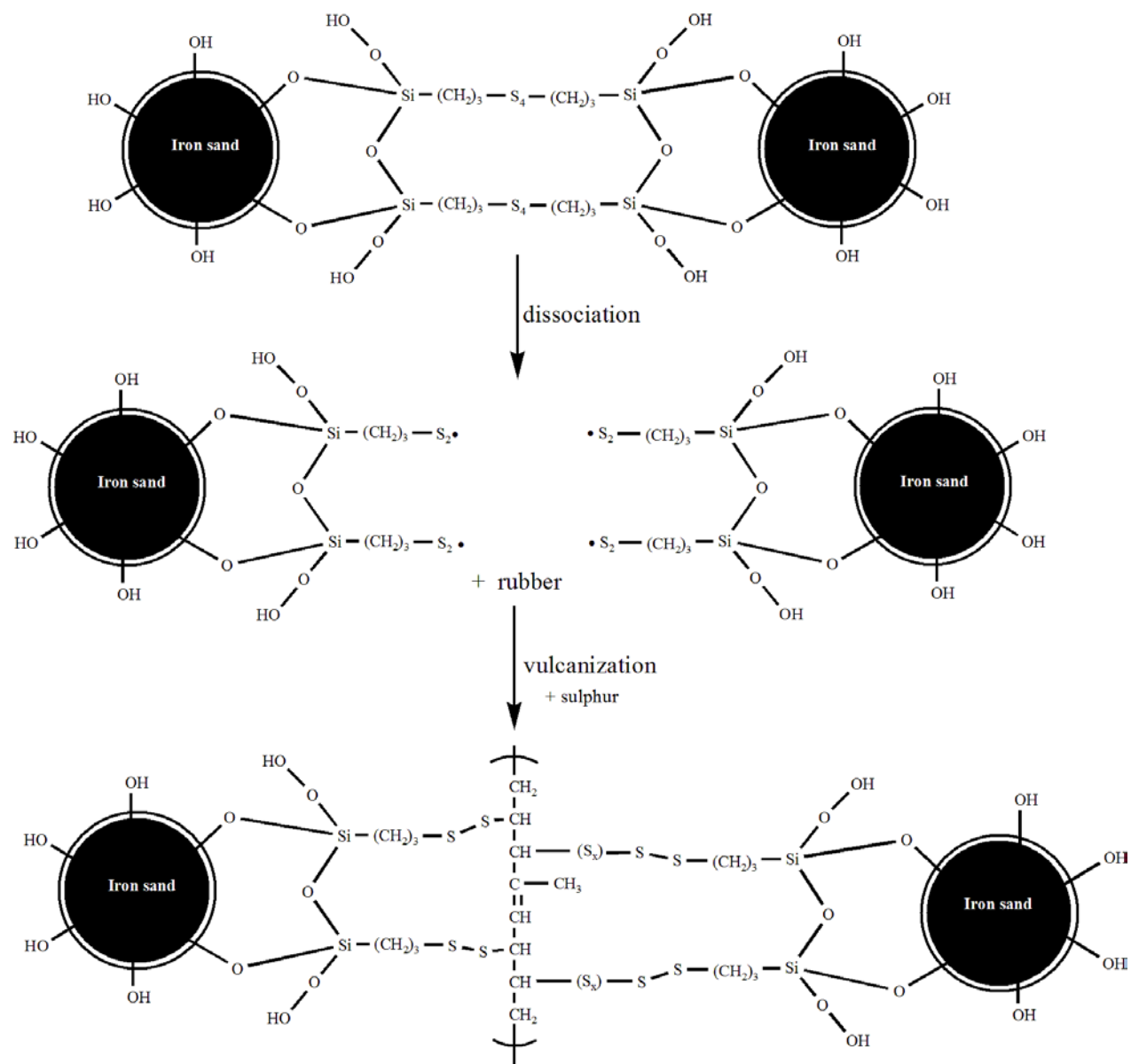


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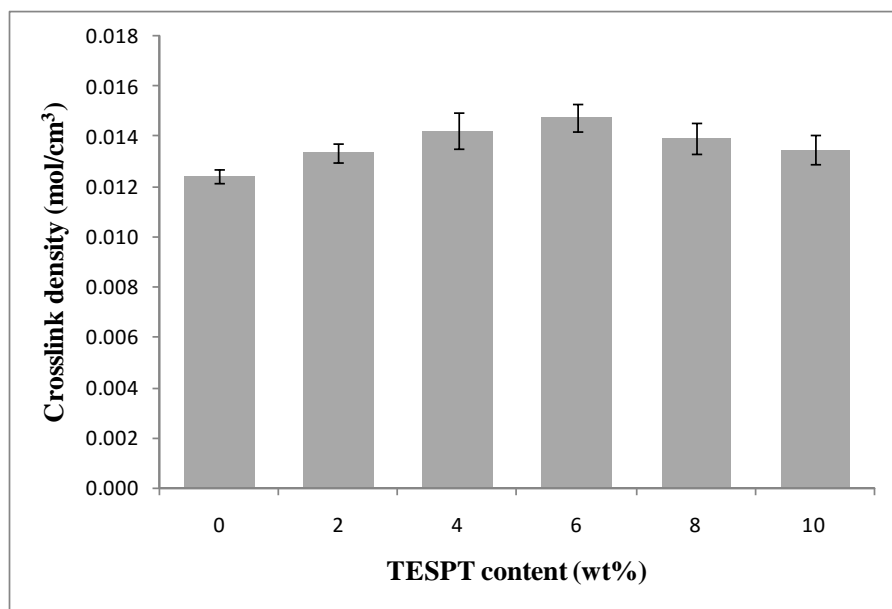


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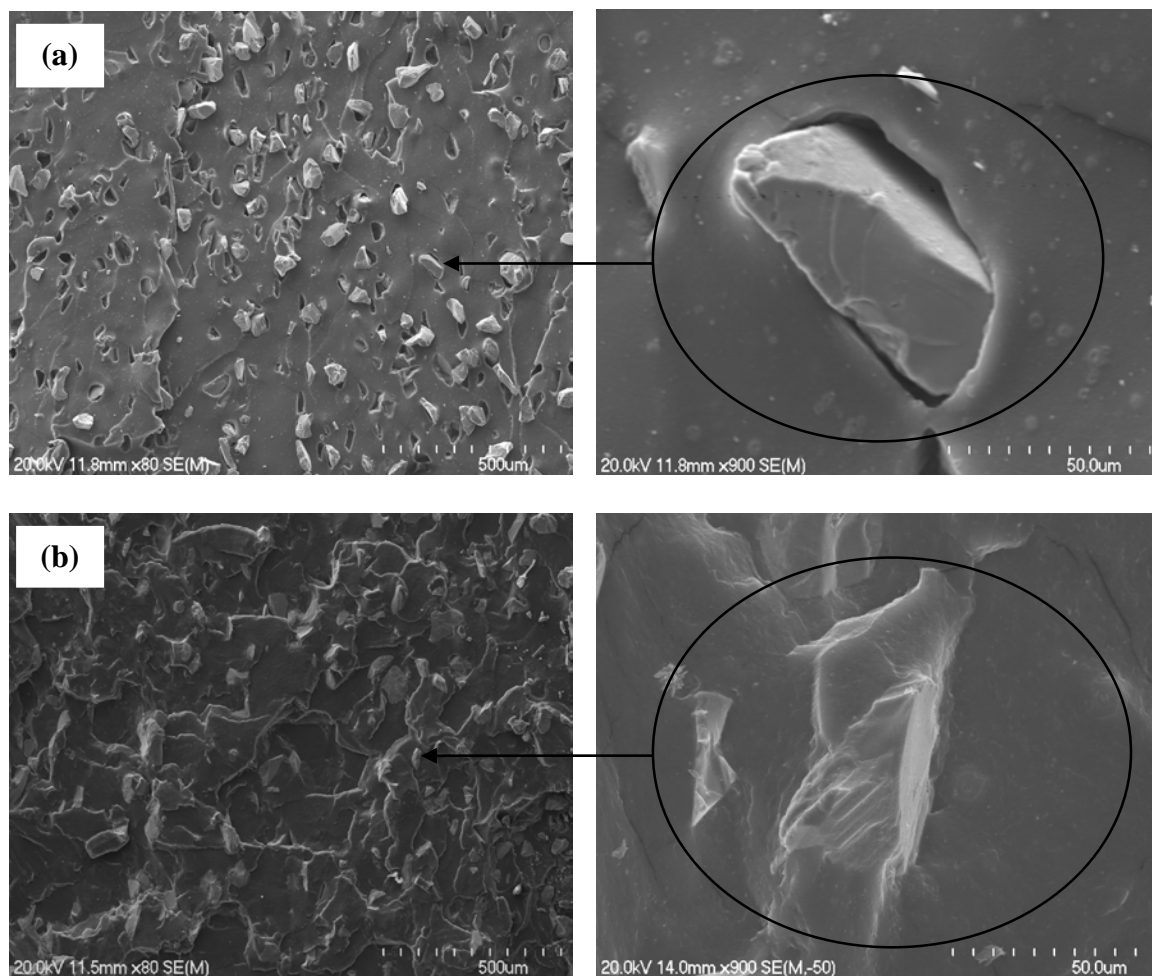


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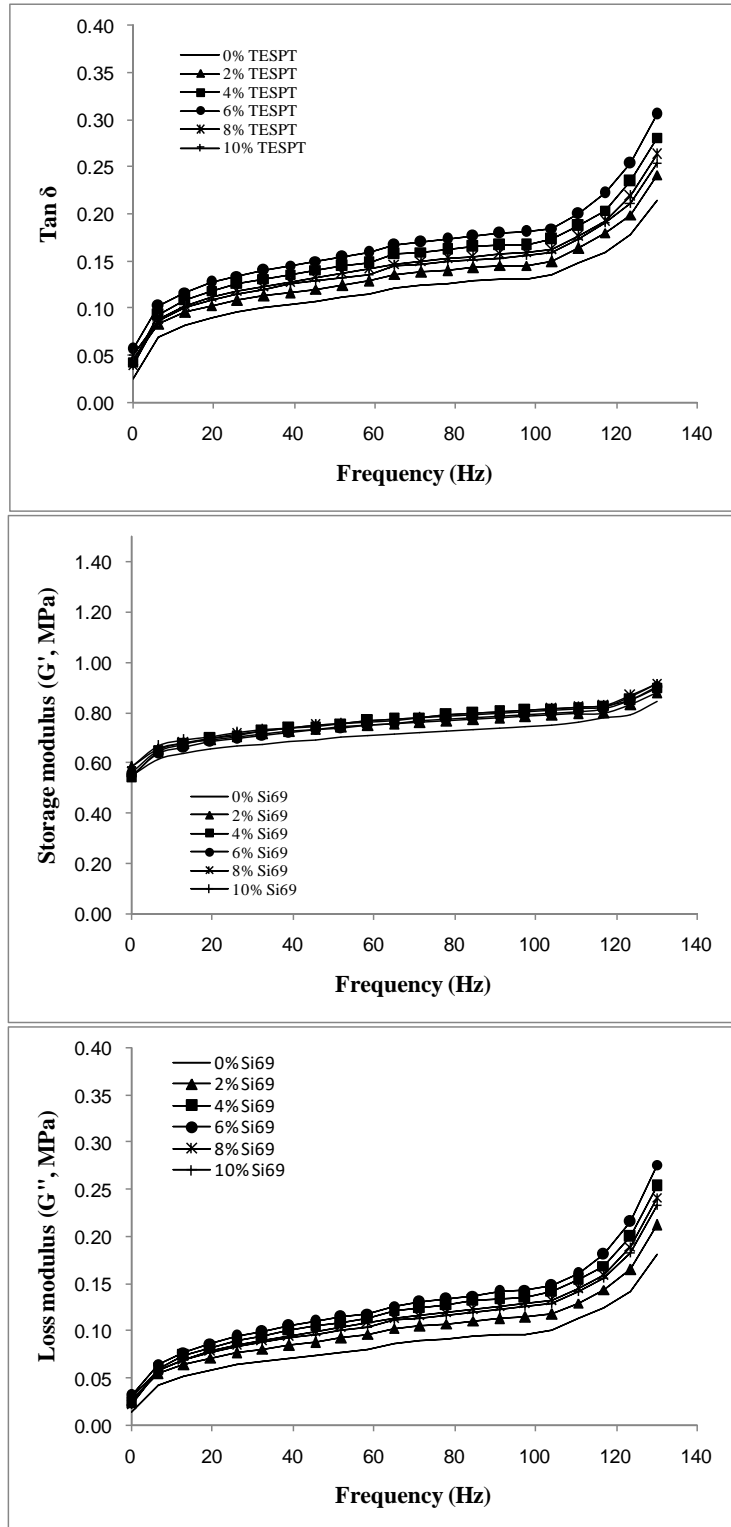


Figure 9

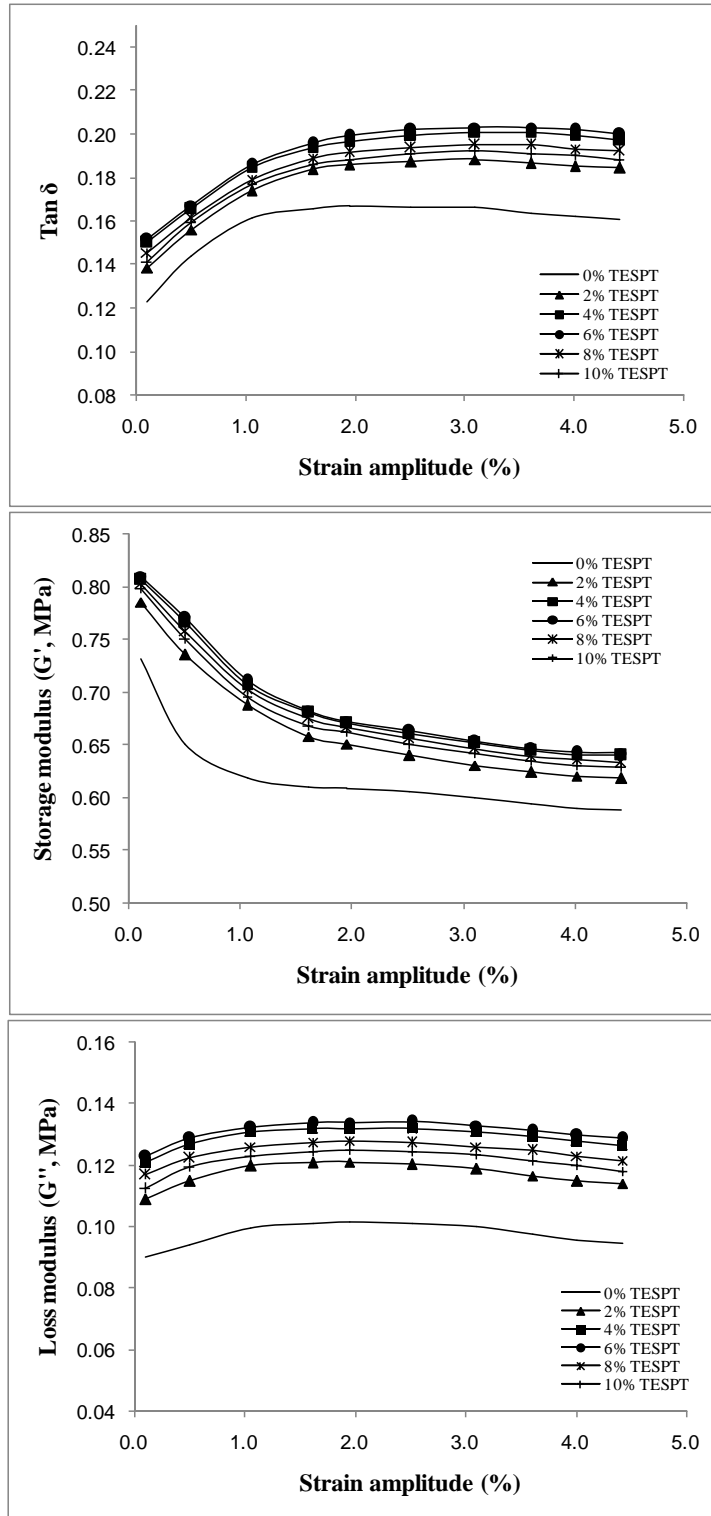


Figure 10

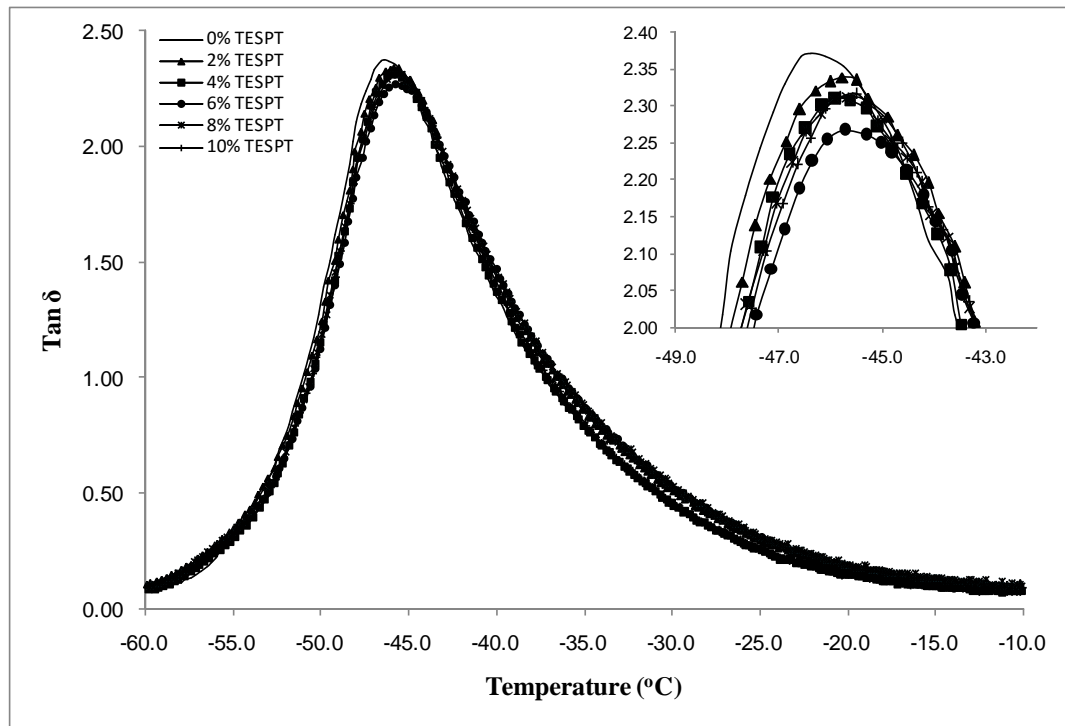


Figure 11

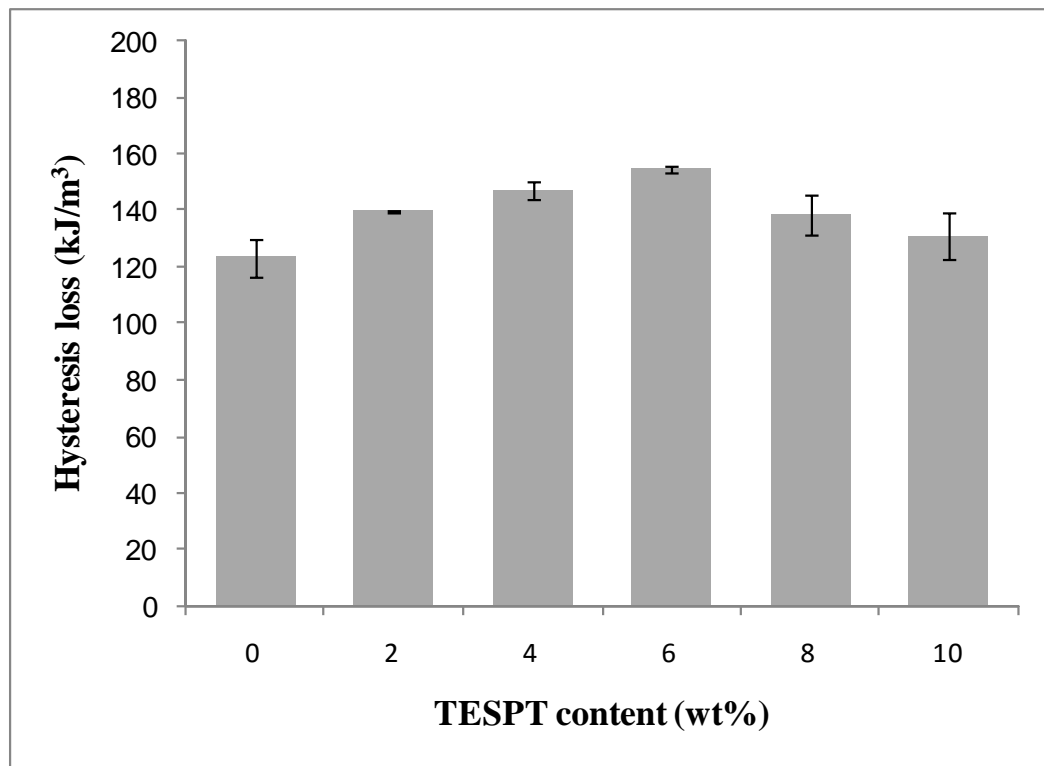


Figure 12