

Numerical performance comparison of different tube cross-sections for heat recovery from particle-laden exhaust gas streams

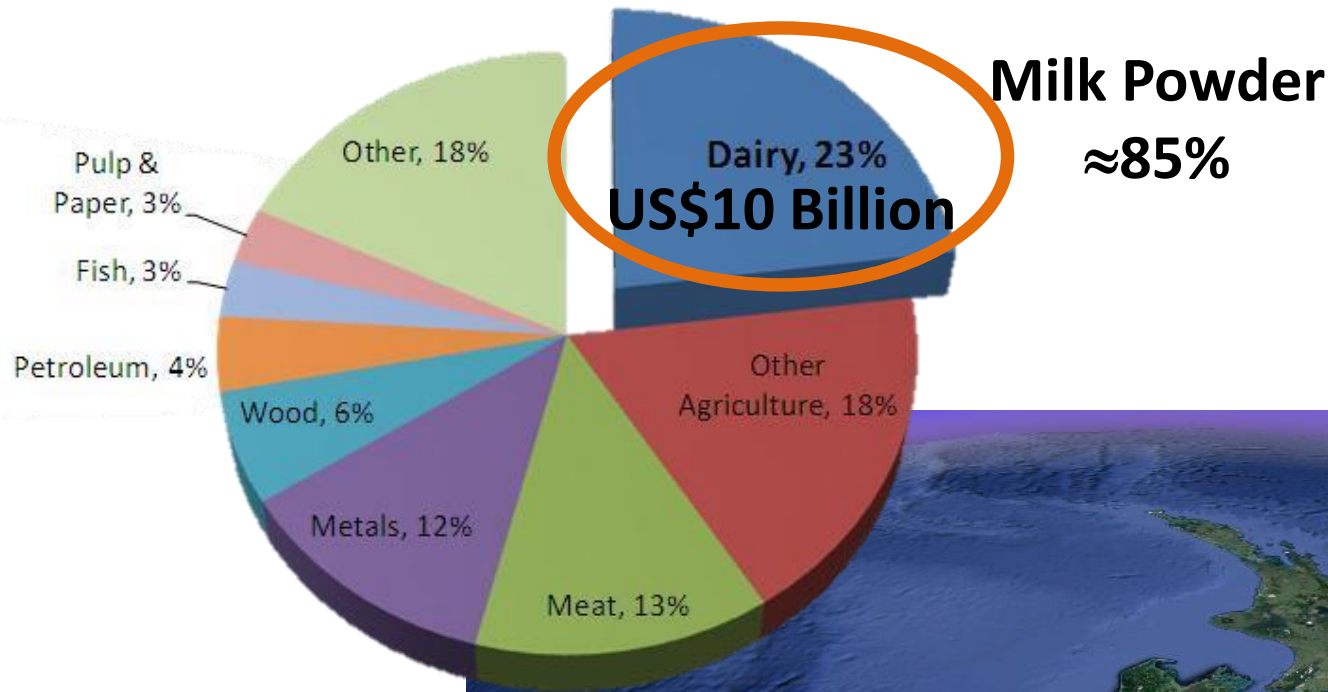
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School of Engineering
University of Waikato
2012**

Outline

- Background
- Challenges facing heat recovery from air
- Methodology
- Numerical Results
- Experimental Work
- Summary

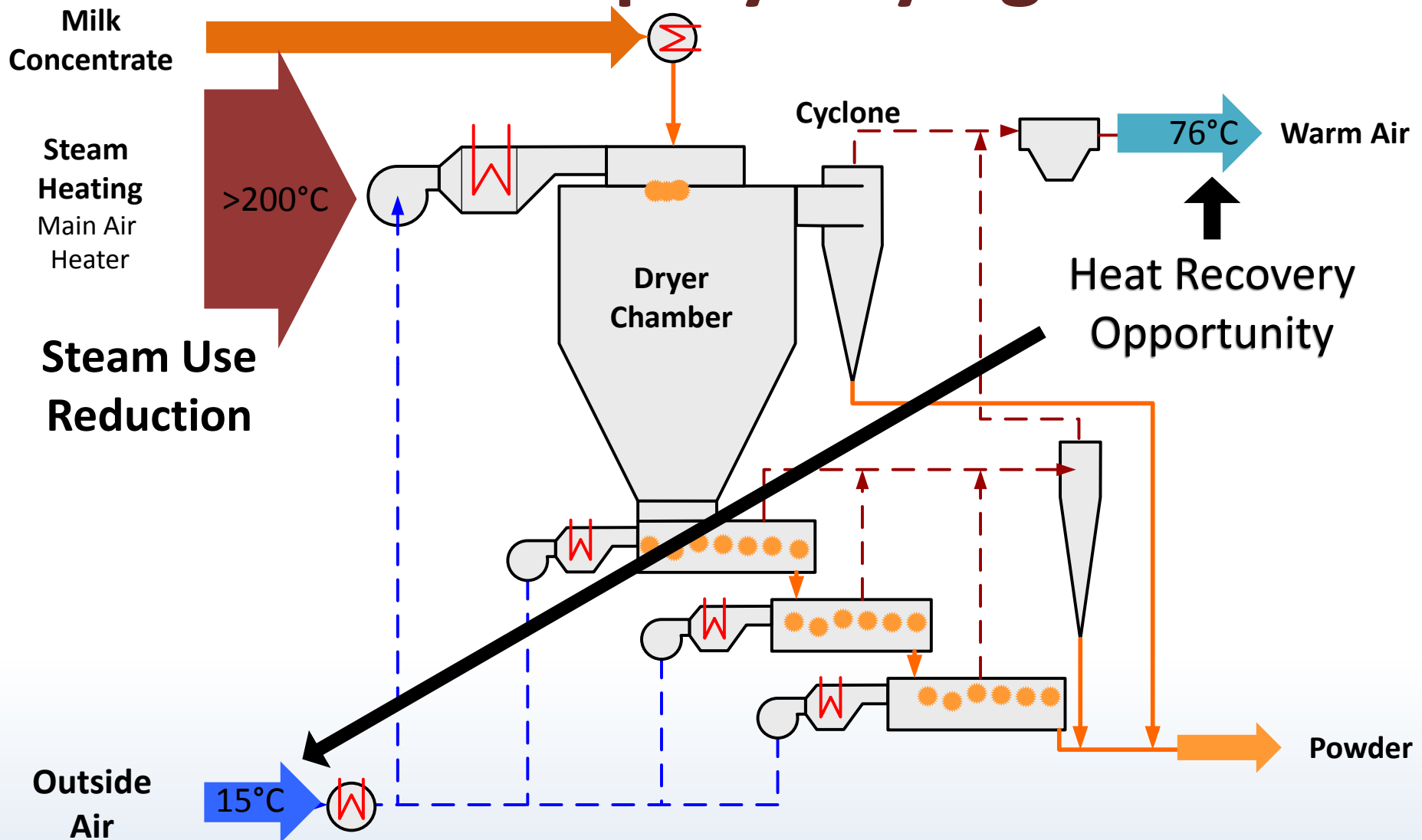
New Zealand Exports



New Zealand Dairy



Milk Spray Drying



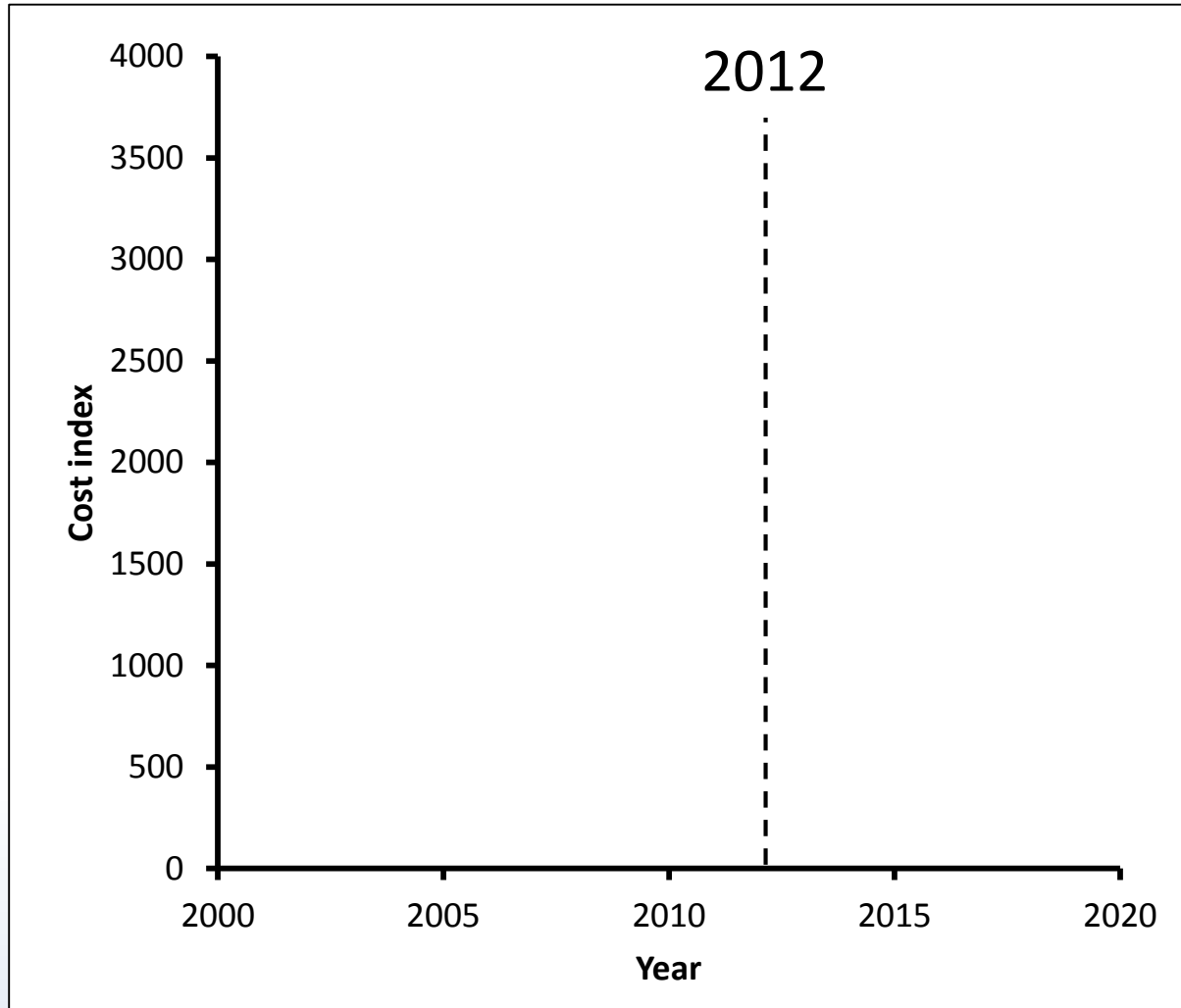
Challenges

- 1) Expensive to recover heat from air
- 2) Distance between exhaust and inlet ducts
- 3) Particulate fouling
- 4) High heat transfer resistance and lots of area

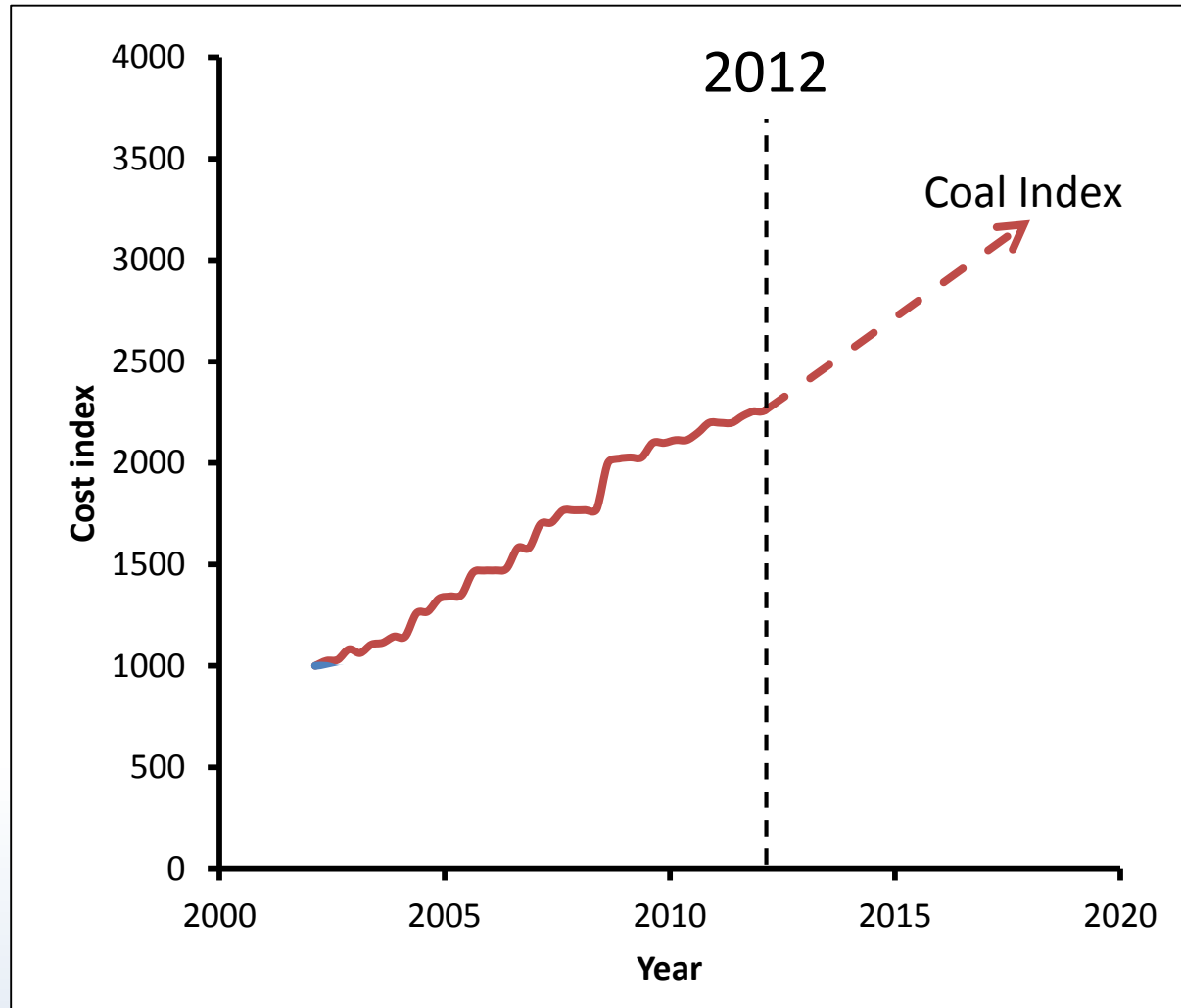
Challenges

- 1) **Expensive to recover heat from air**
- 2) Distance between exhaust and inlet ducts
- 3) Particulate fouling
- 4) High heat transfer resistance and lots of area

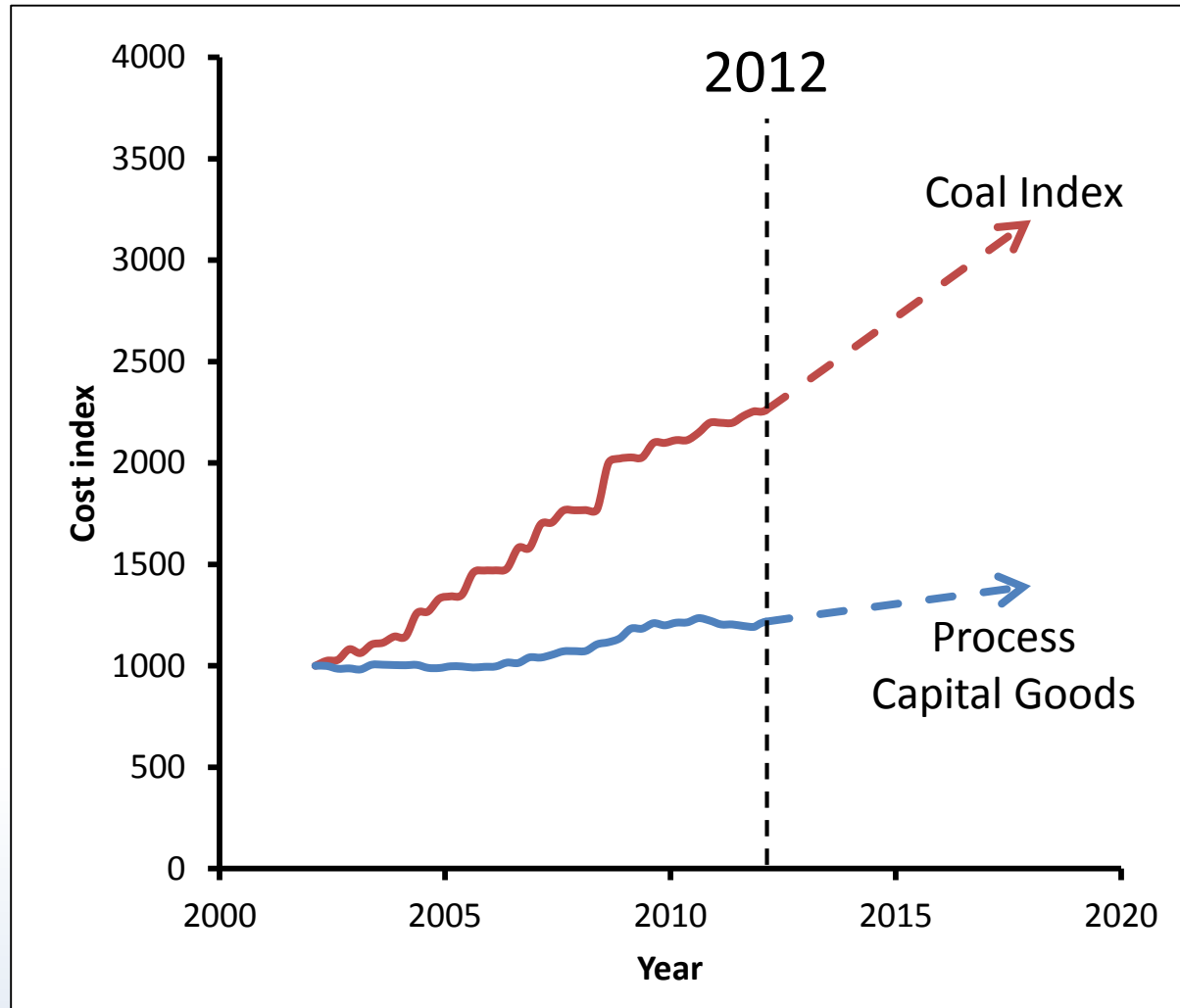
How Fast are Steam Prices Rising?



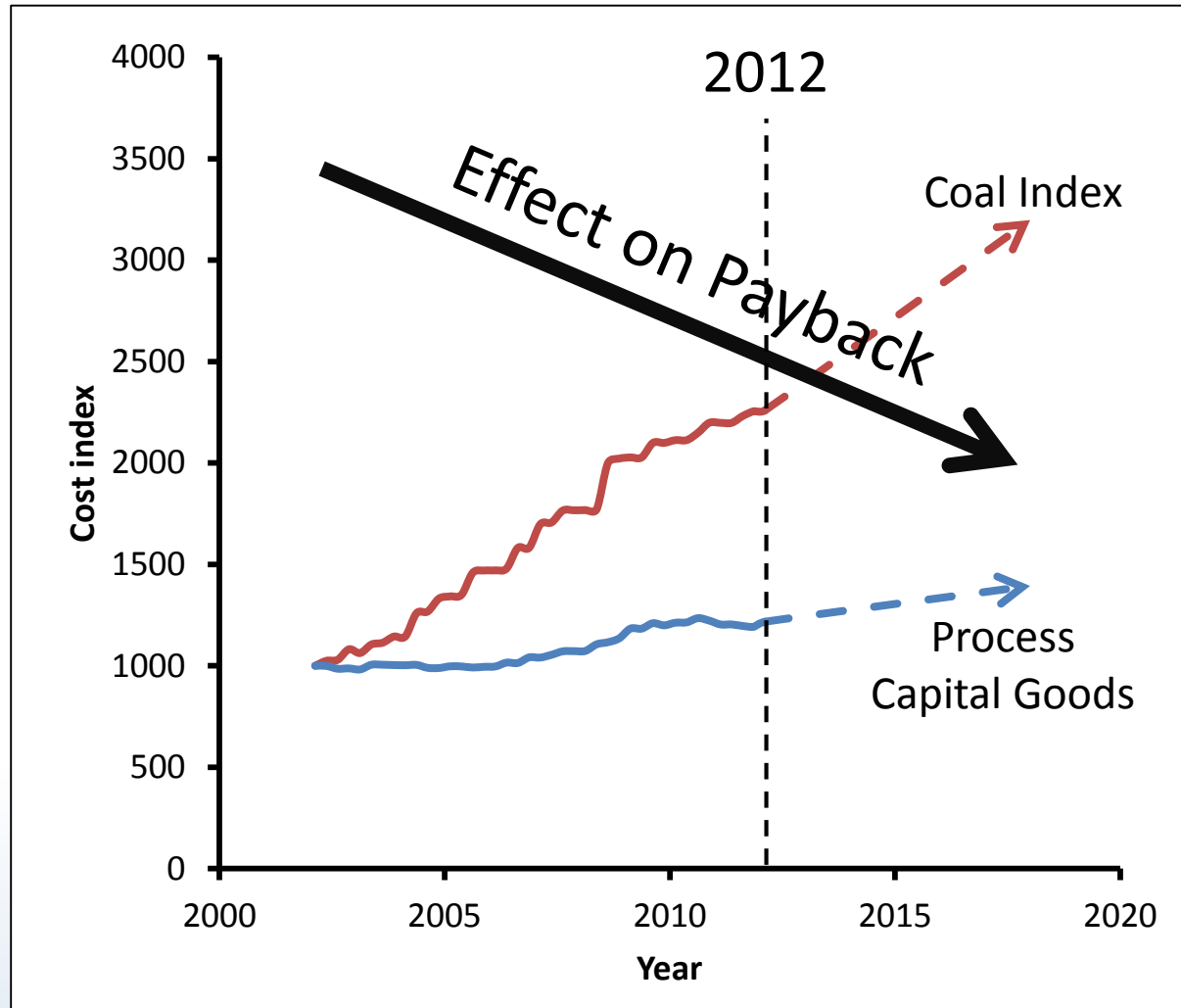
How Fast are Steam Prices Rising?



How Fast are Steam Prices Rising?



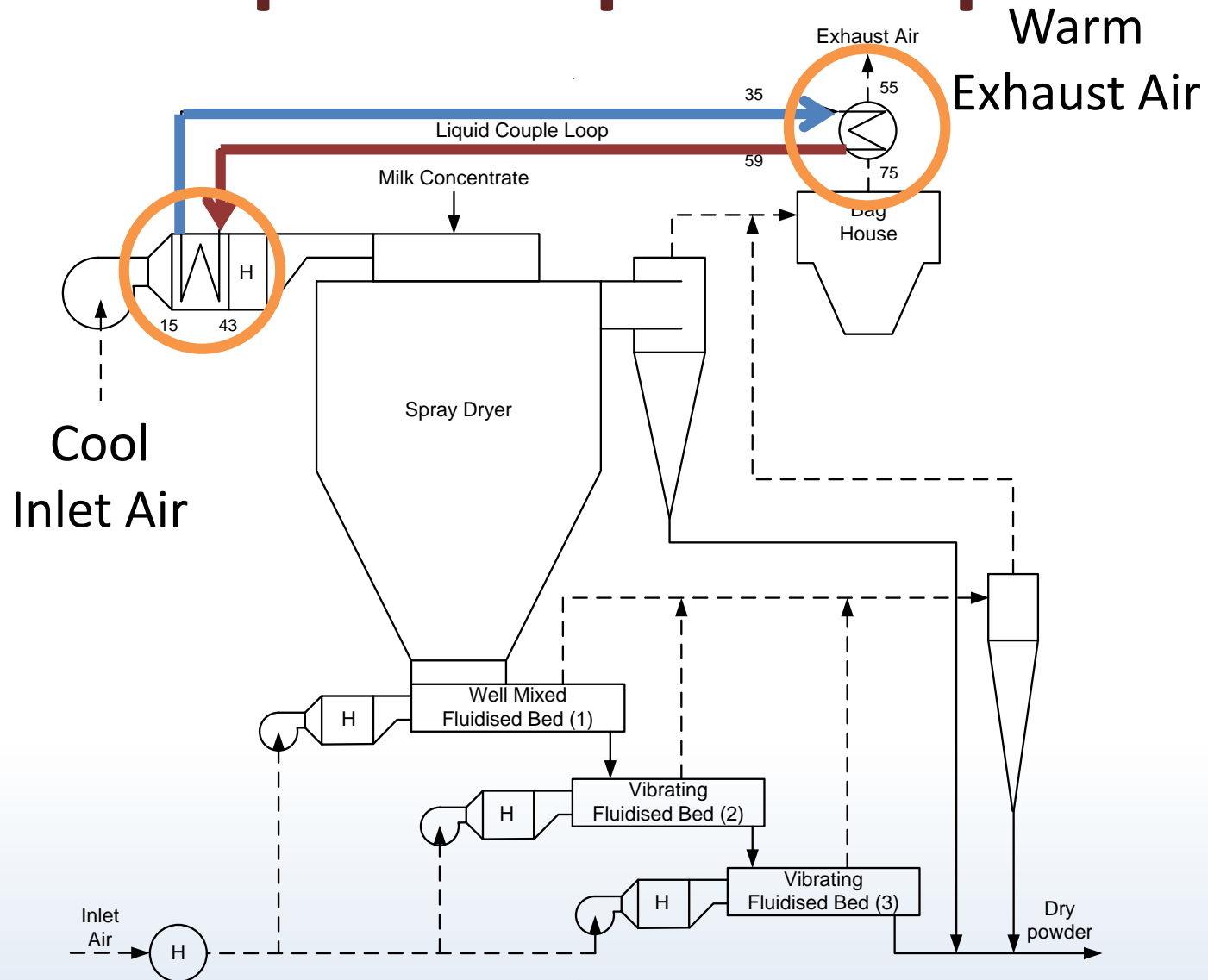
How Fast are Steam Prices Rising?



Challenges

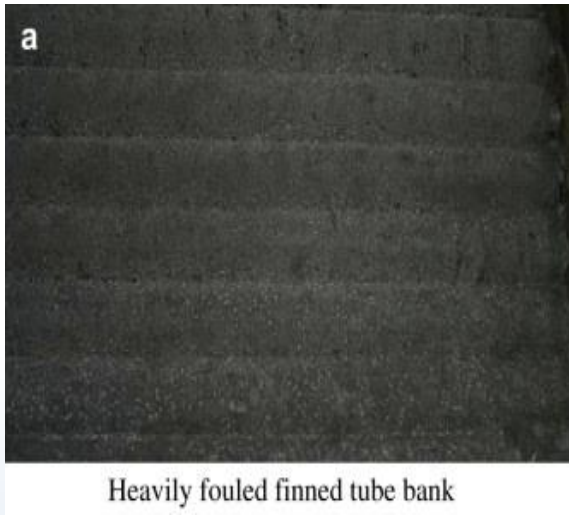
- 1) Expensive to recover heat from air
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Liquid Coupled Loop



Challenges

- 1) Expensive to recover heat from air
- 2) Distance between exhaust and inlet ducts
- 3) Particulate fouling**
- 4) High heat transfer resistance and lots of area



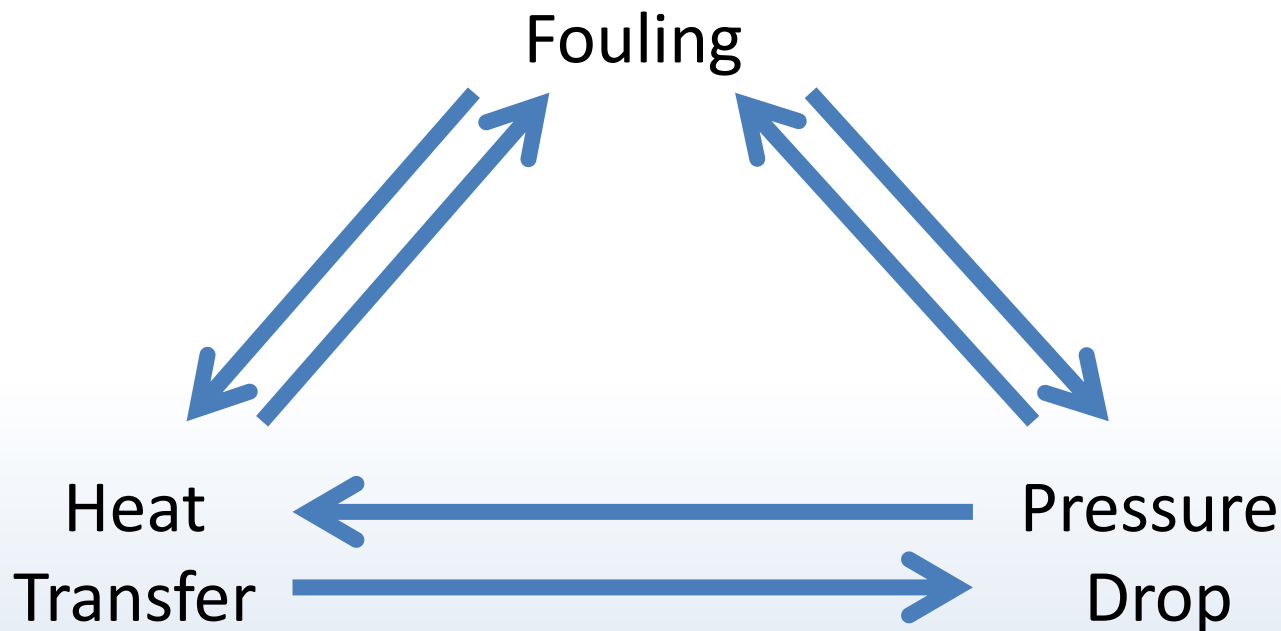
Finned Tube Boiler Recuperator



Inside a Dairy Plant

Challenges

- 1) Expensive to recover heat from air
- 2) Distance between exhaust and inlet ducts
- 3) Particulates
- 4) **High heat transfer resistance and lots of area**



What is the General Solution?

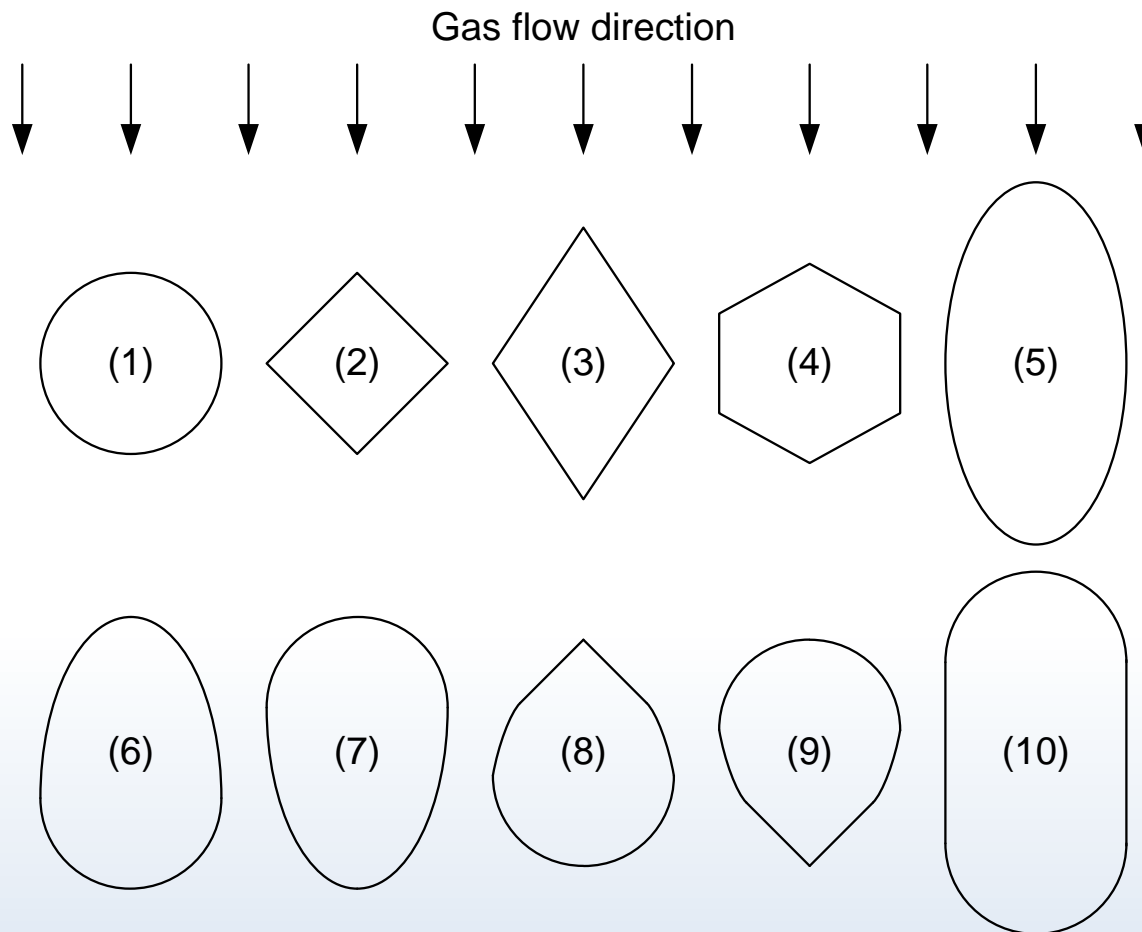
- Liquid coupled loop of compact HX
- Inlet exchanger can use finned tube compact HX
- Exhaust exchanger needs to be low fouling – no extended surface fins
 - Bare tube
 - Plain plate HX (not considered in this paper)

**THEREFORE, WHAT IS
THE BEST TUBE SHAPE?**



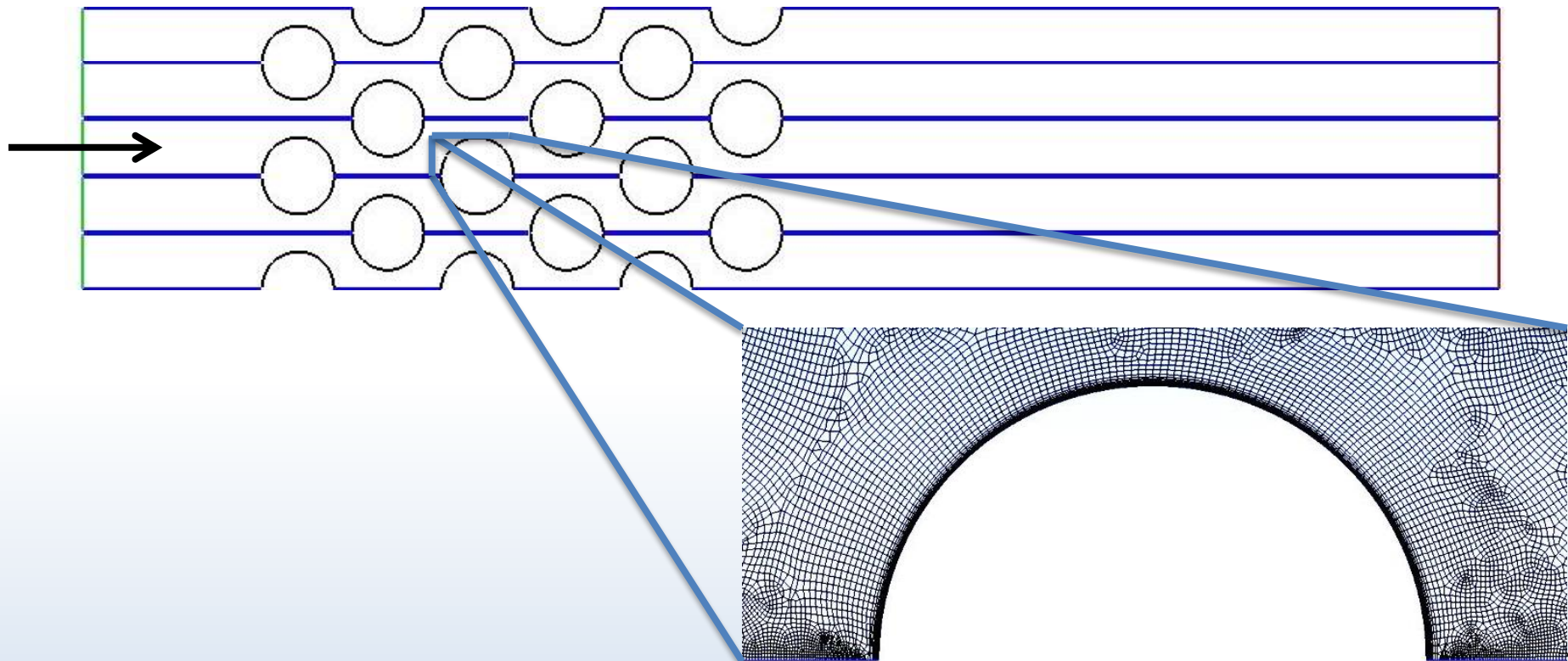
Methodology

- Selected 10 common shapes



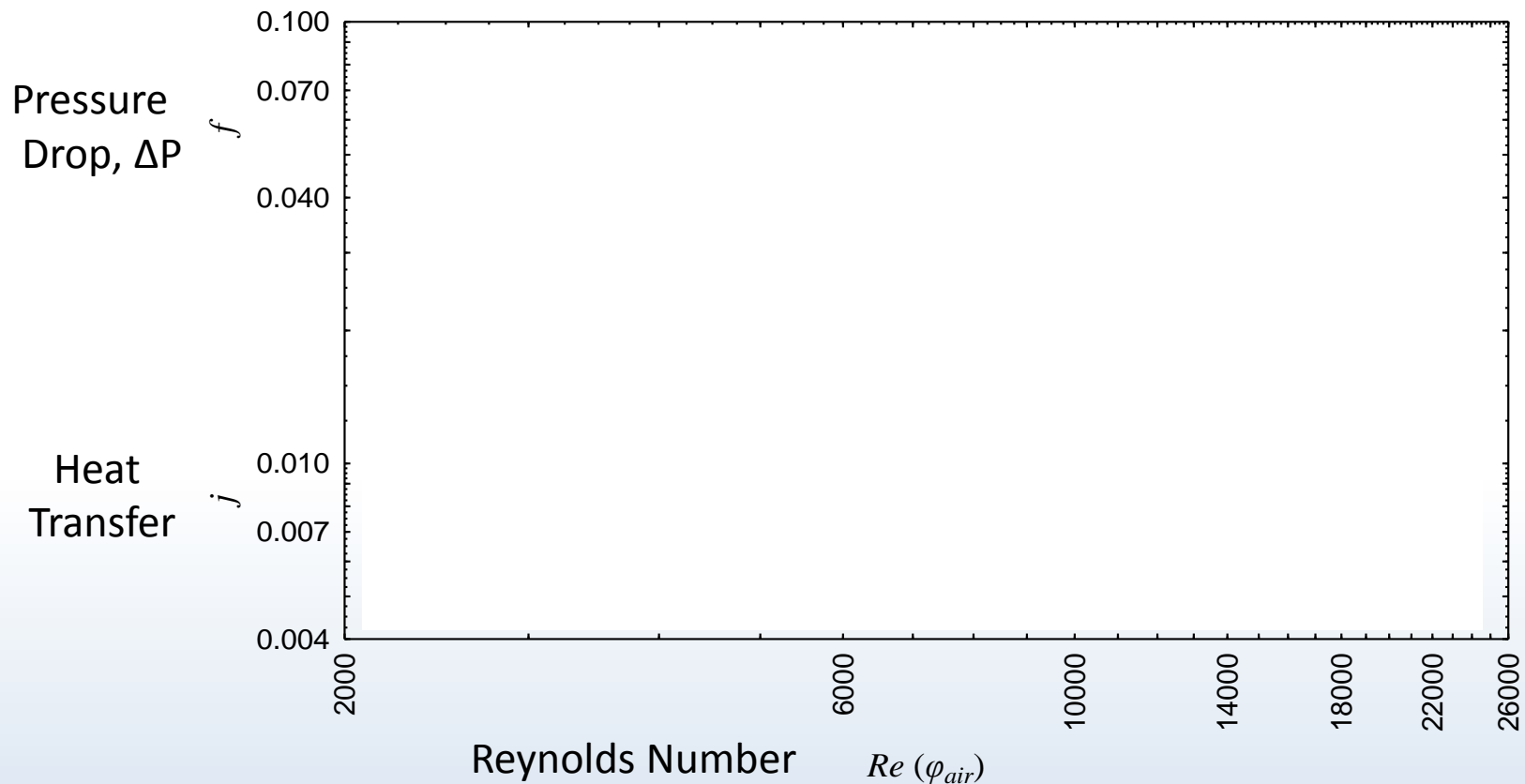
Methodology

- Constructed CFD models in Fluent 13.0, 6 rows
 - Constant free-flow, σ
 - Constant HT area / volume, α , (changing length spacing)



Methodology

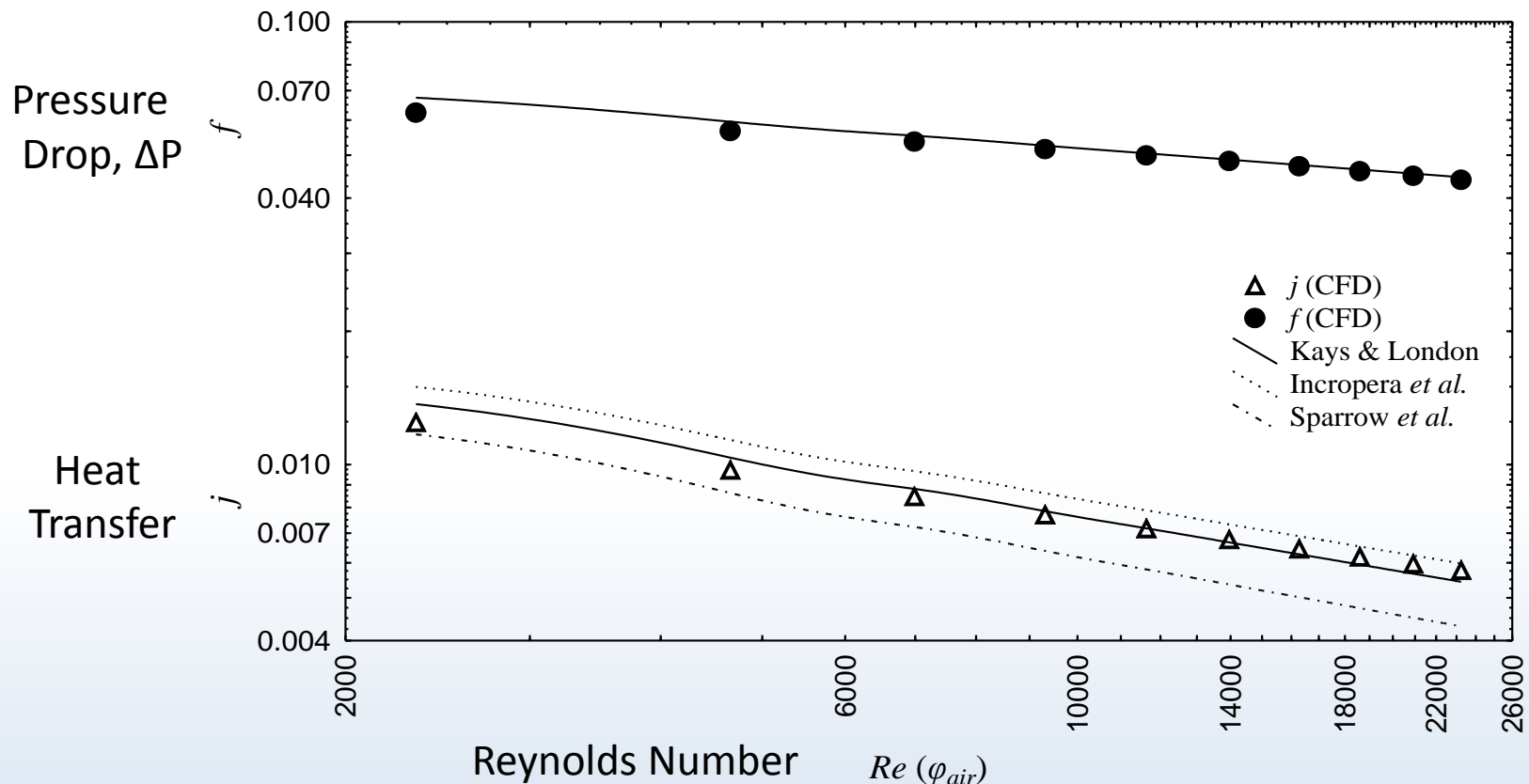
- Compared models to experimental correlations (if available)
 - Round tube



Methodology

- Compared models to experimental correlations (if available)

– Round tube



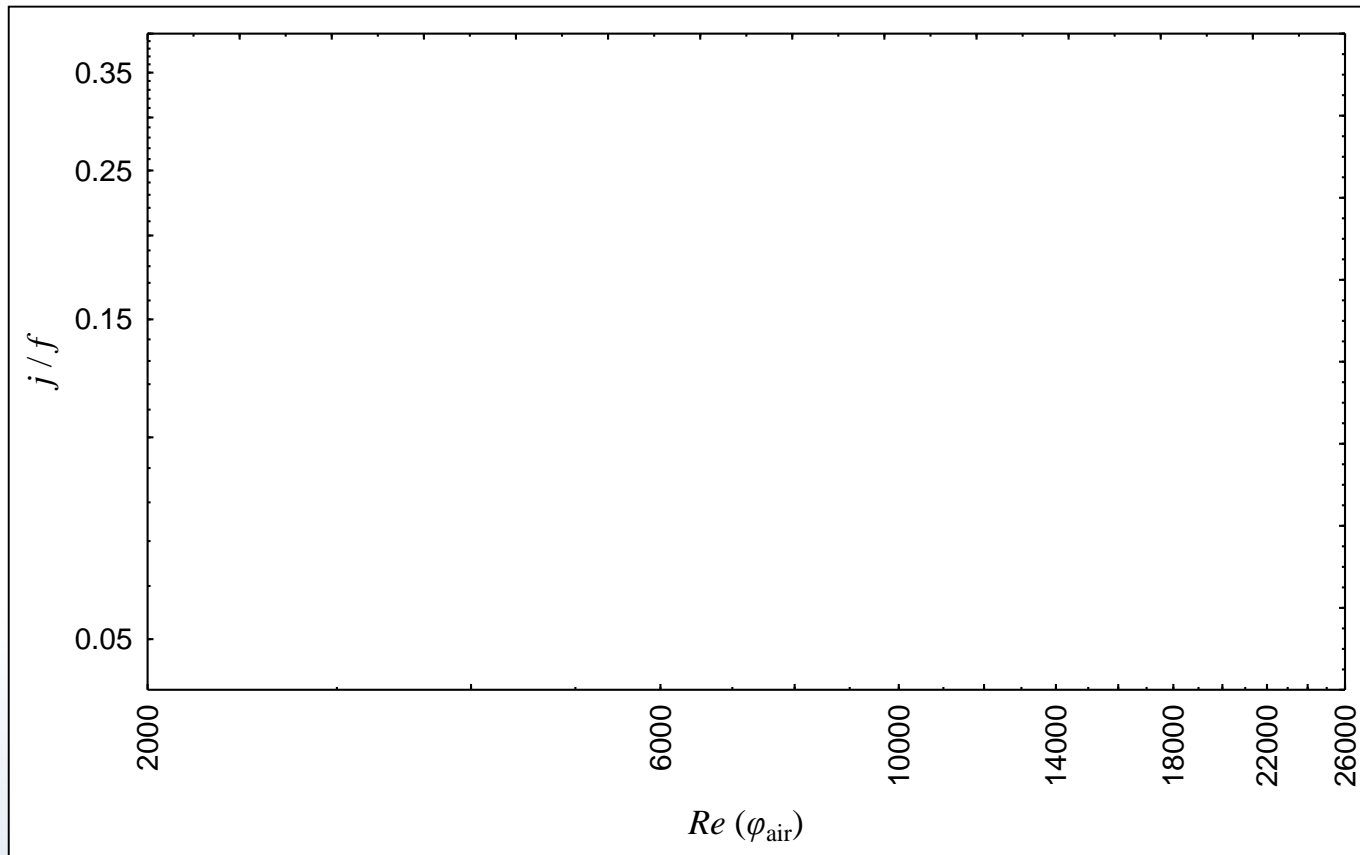
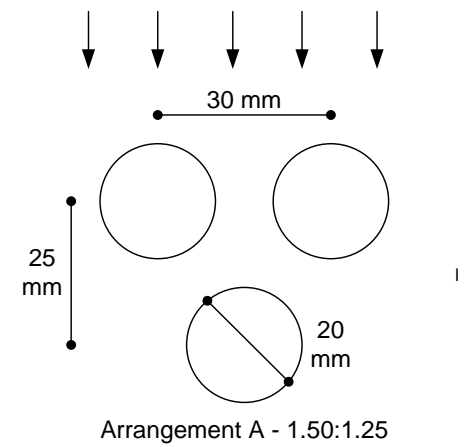
Basis for Comparison

1. Heat transfer coefficient per unit fan power
(Kays & London, 1998)

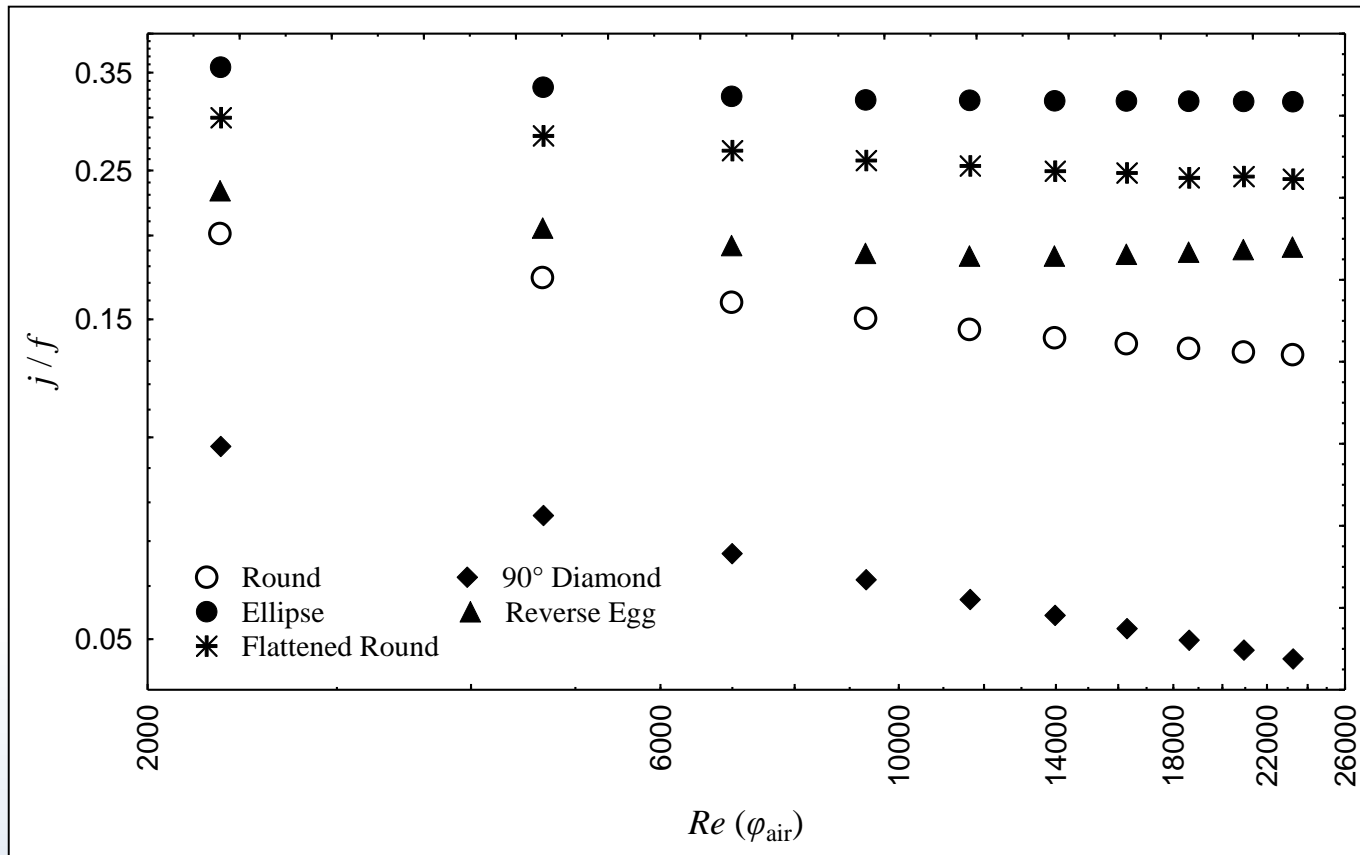
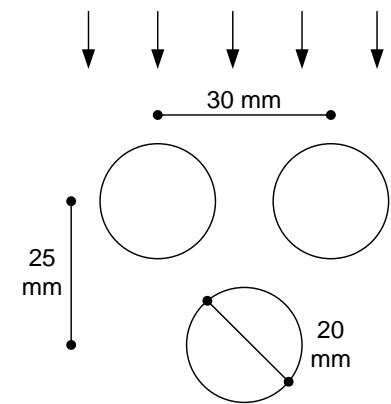
– $h/E \propto \sigma^2 j/f$

– Compare tubes with the same σ and α

Results



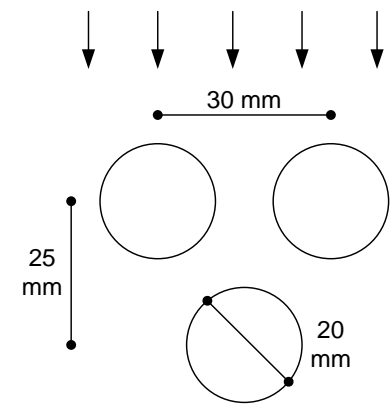
Results



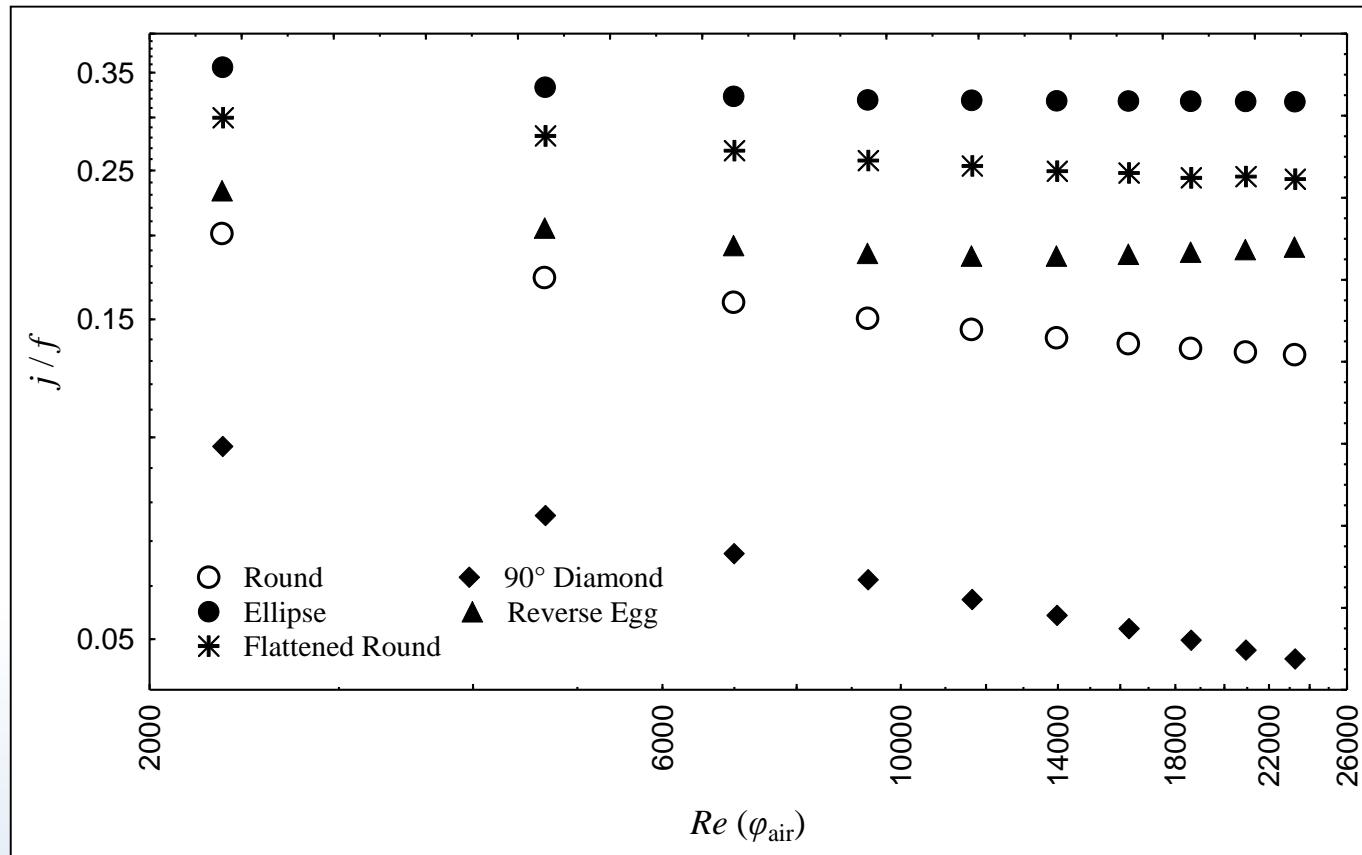
Efficiency Ranking

1. Elliptical
2. Flattened round
3. Reverse egg

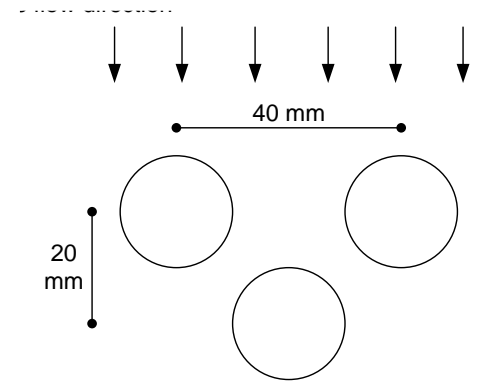
Results



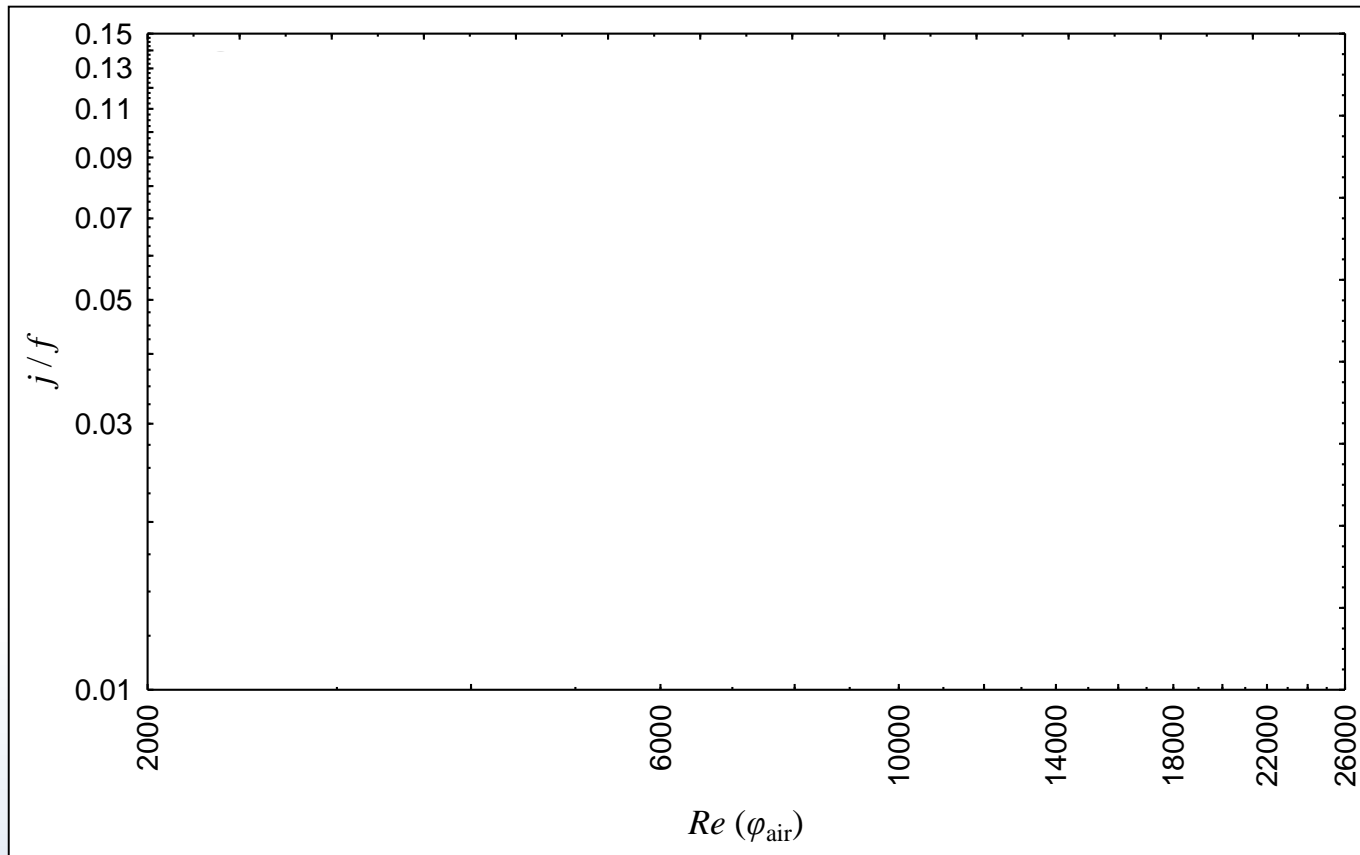
Arrangement A - 1.50:1.25



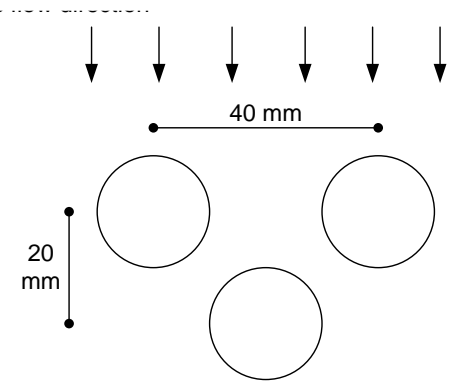
Results



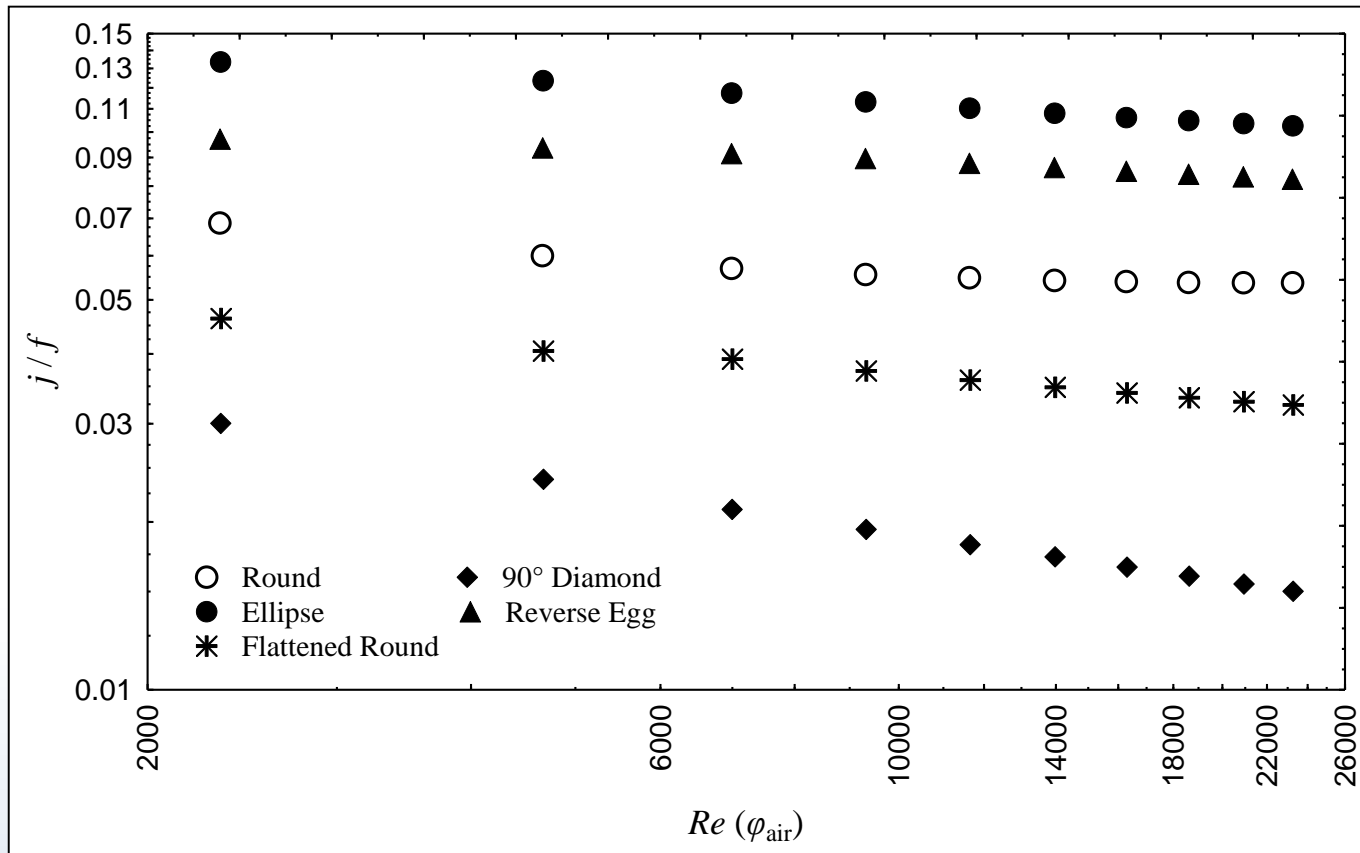
Arrangement B - 2.00:1.00



Results



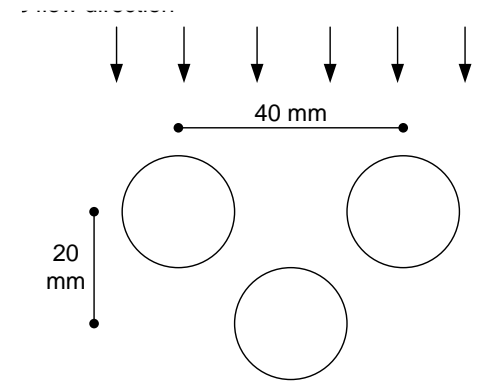
Arrangement B - 2.00:1.00



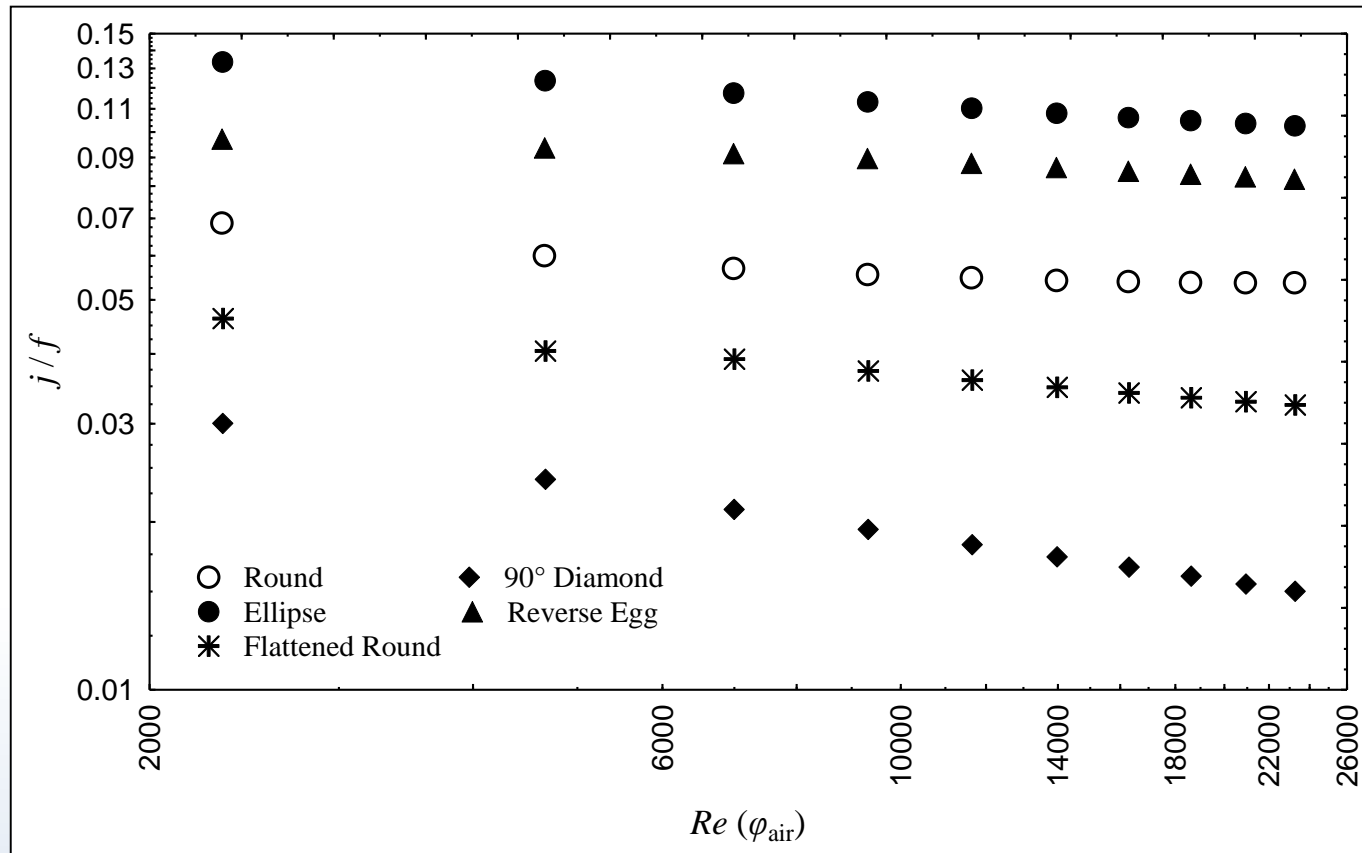
Efficiency Ranking

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3. Round

Results



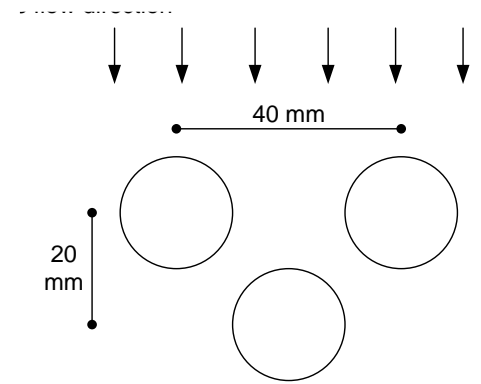
Arrangement B - 2.00:1.00



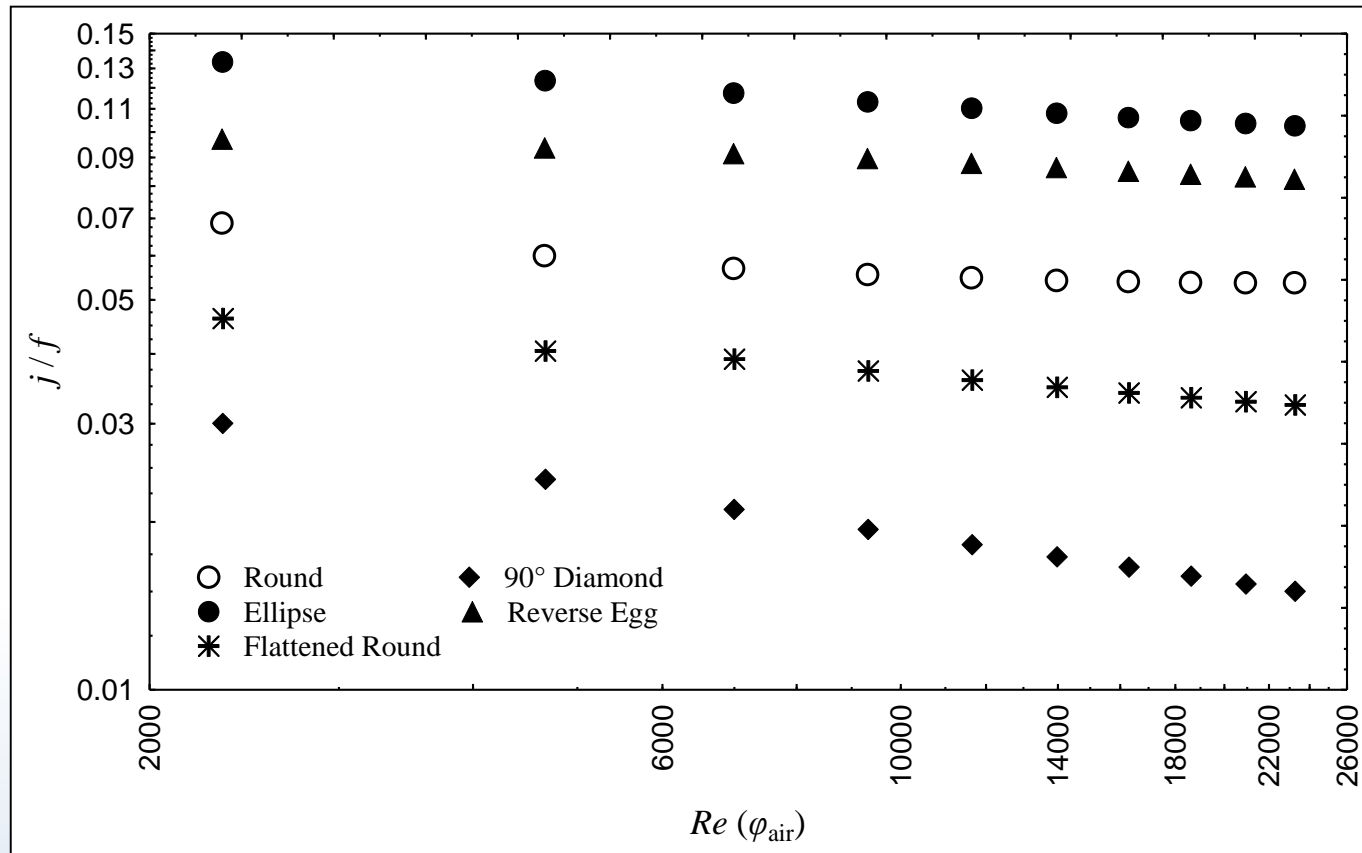
Efficiency Ranking

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Results



Arrangement B - 2.00:1.00



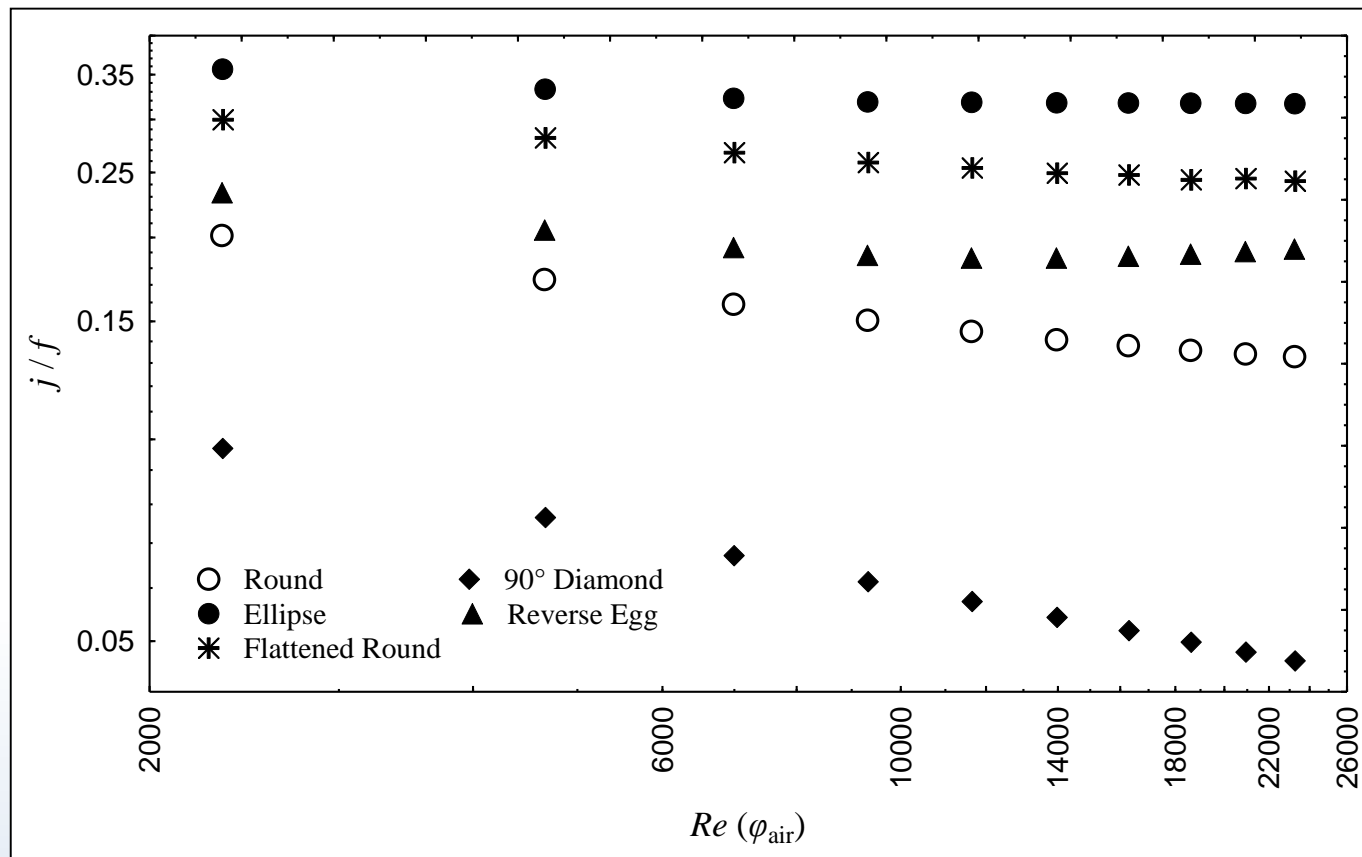
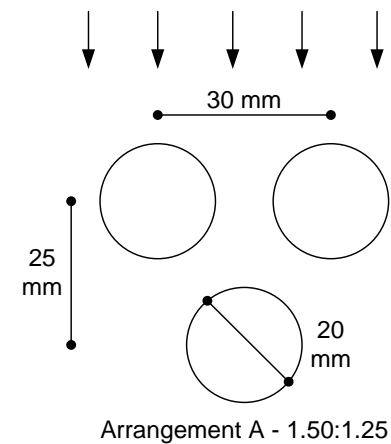
Flattened
Round



Efficiency Ranking

1. Elliptical
2. Flattened round
3. Reverse egg

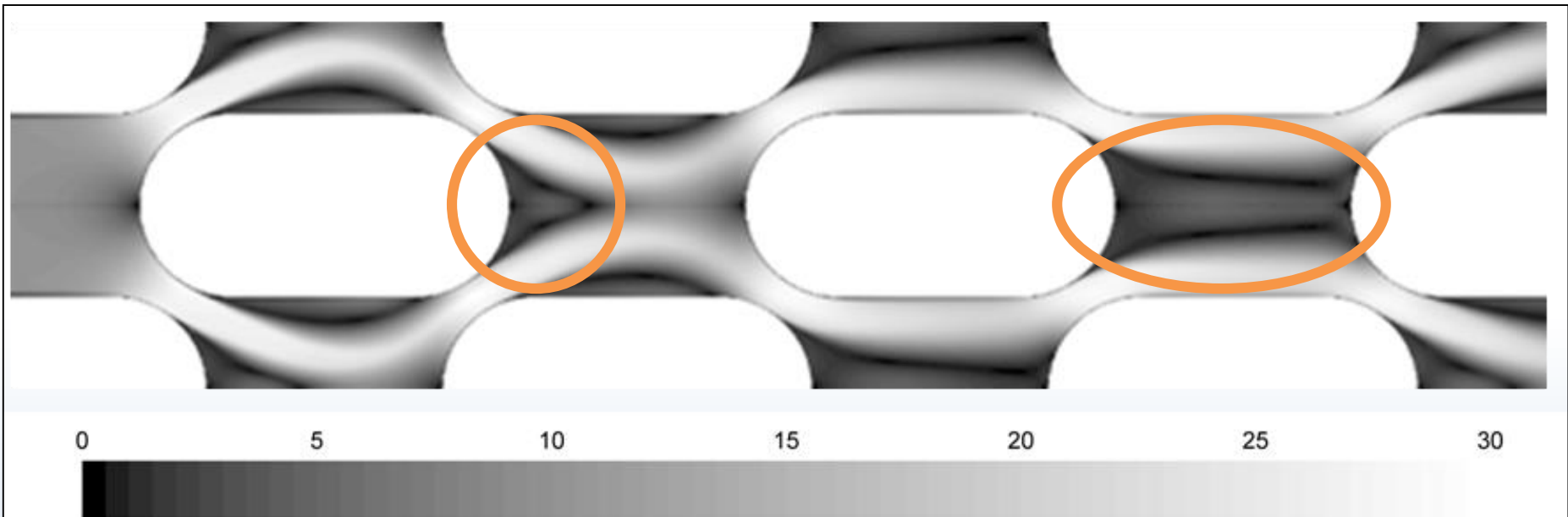
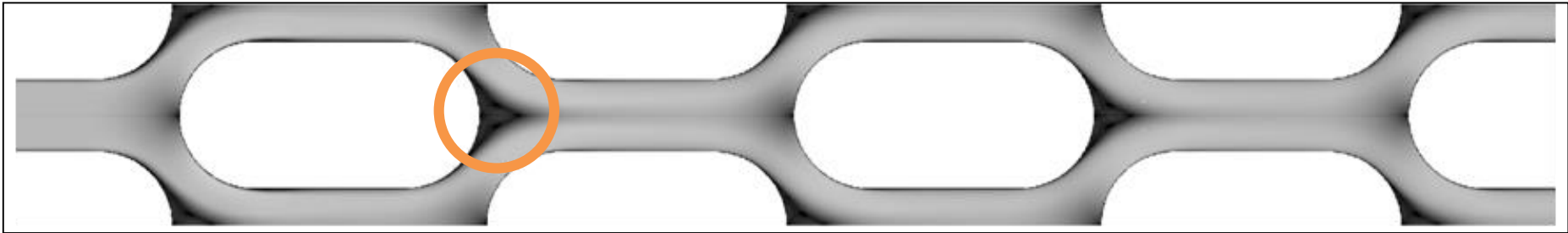
Results



Flattened Round



Optimal Spacing is Important

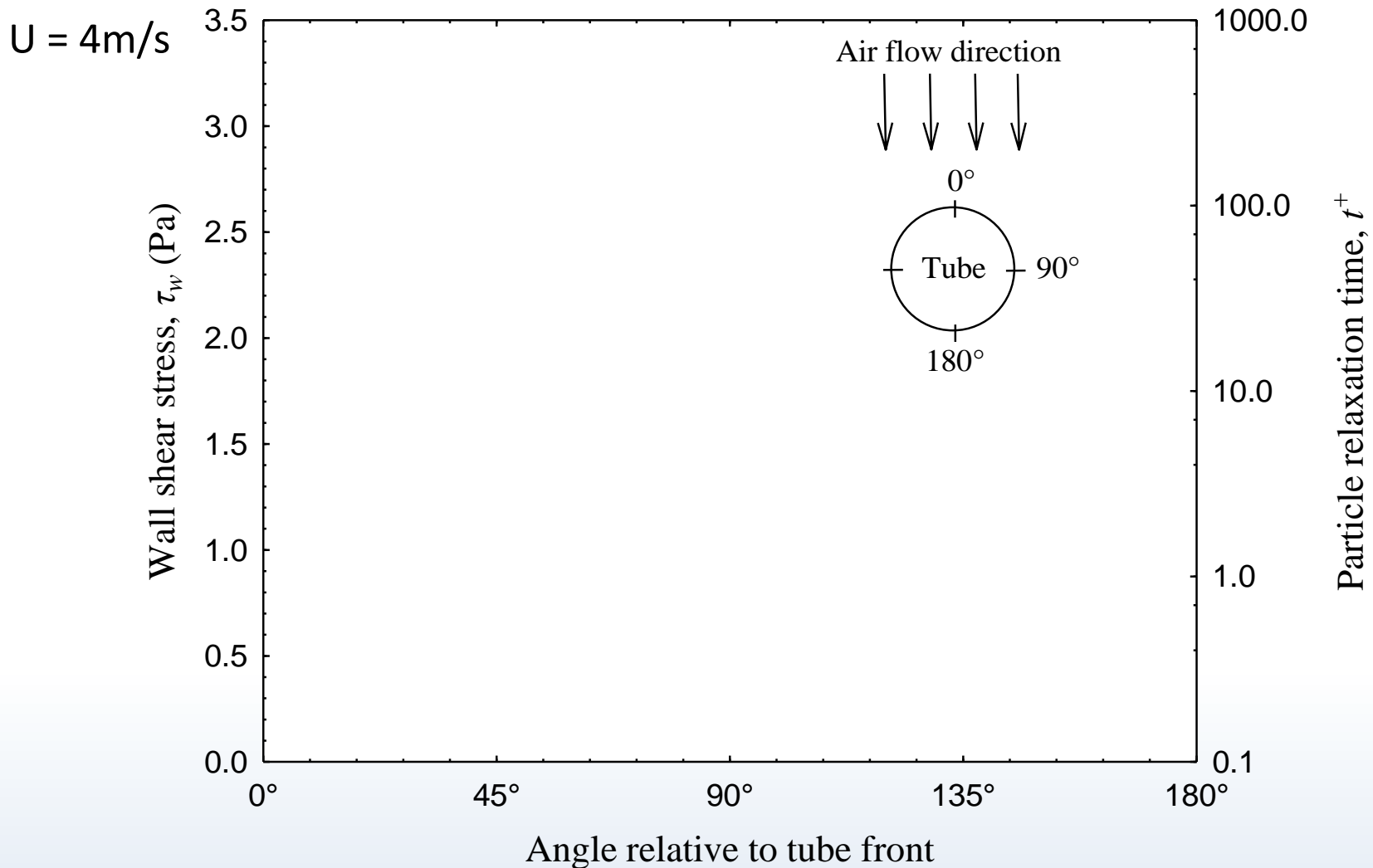


Basis for Comparison

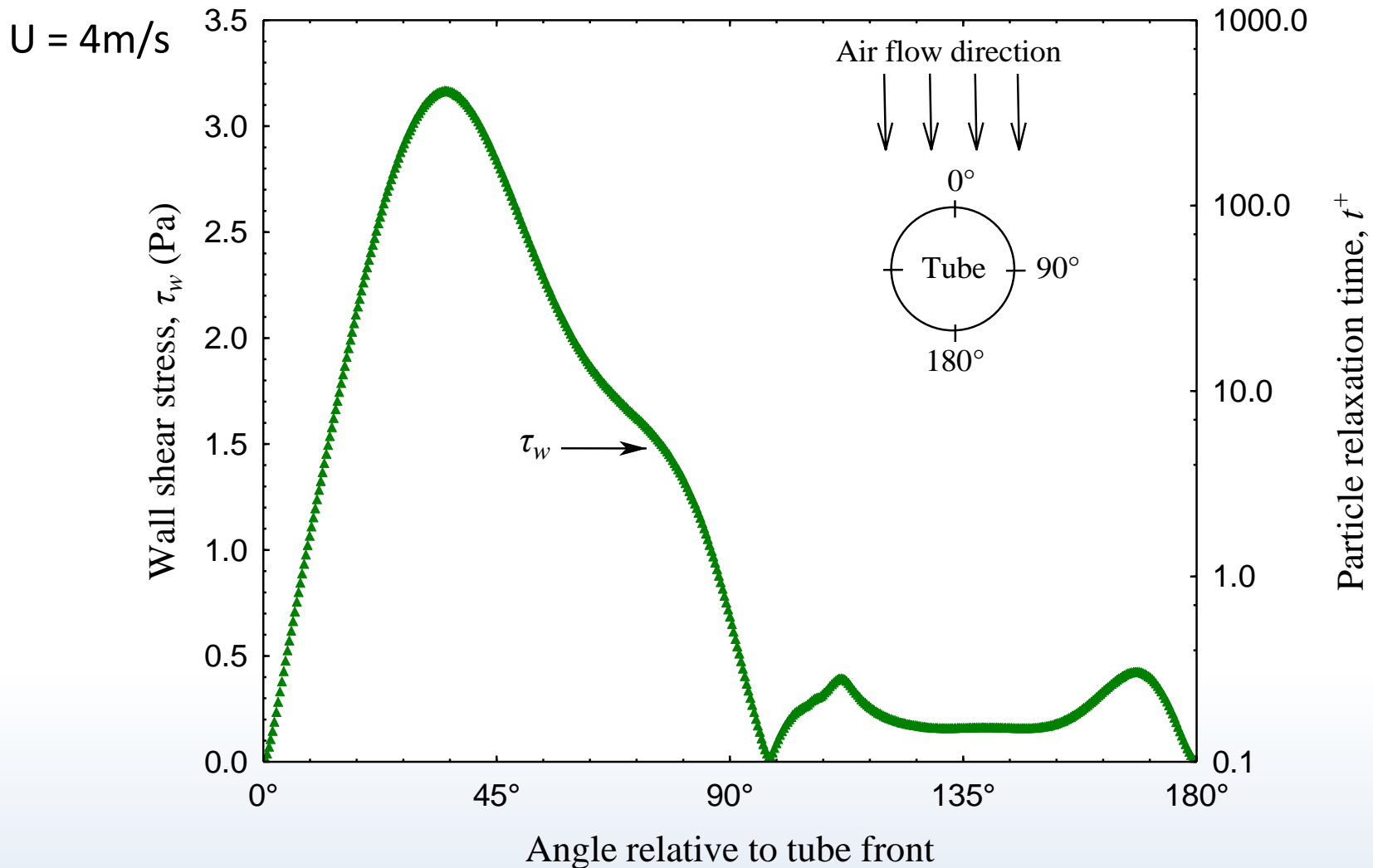
2. Low fouling

- High wall shear stress (related to tube geometry, arrangement and gas flow velocity)
- $R_f \propto 1/\tau_w$
- Adhesion/stickiness properties are important
- These are assumed constant between shapes

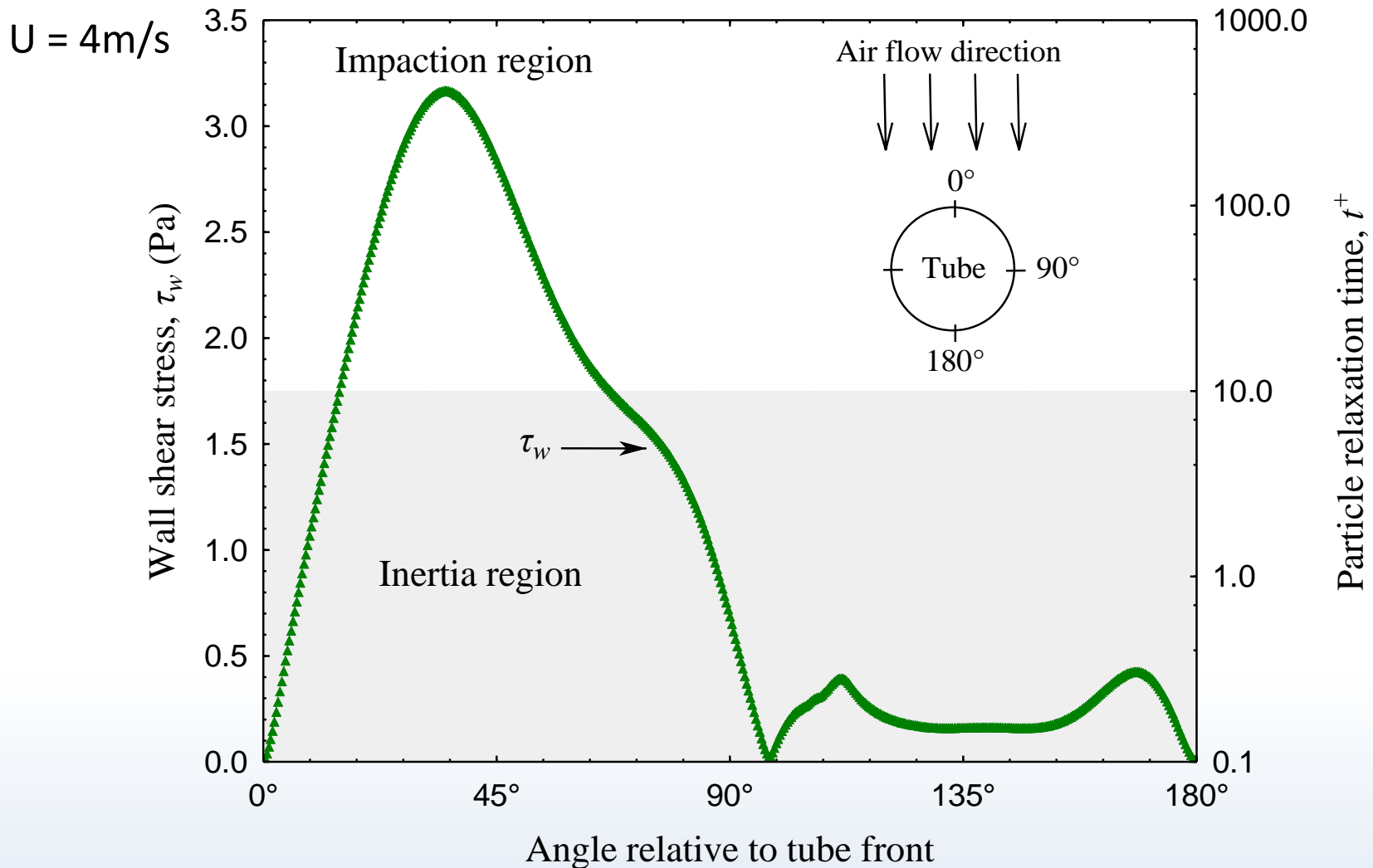
Wall Shear Stress and Deposition



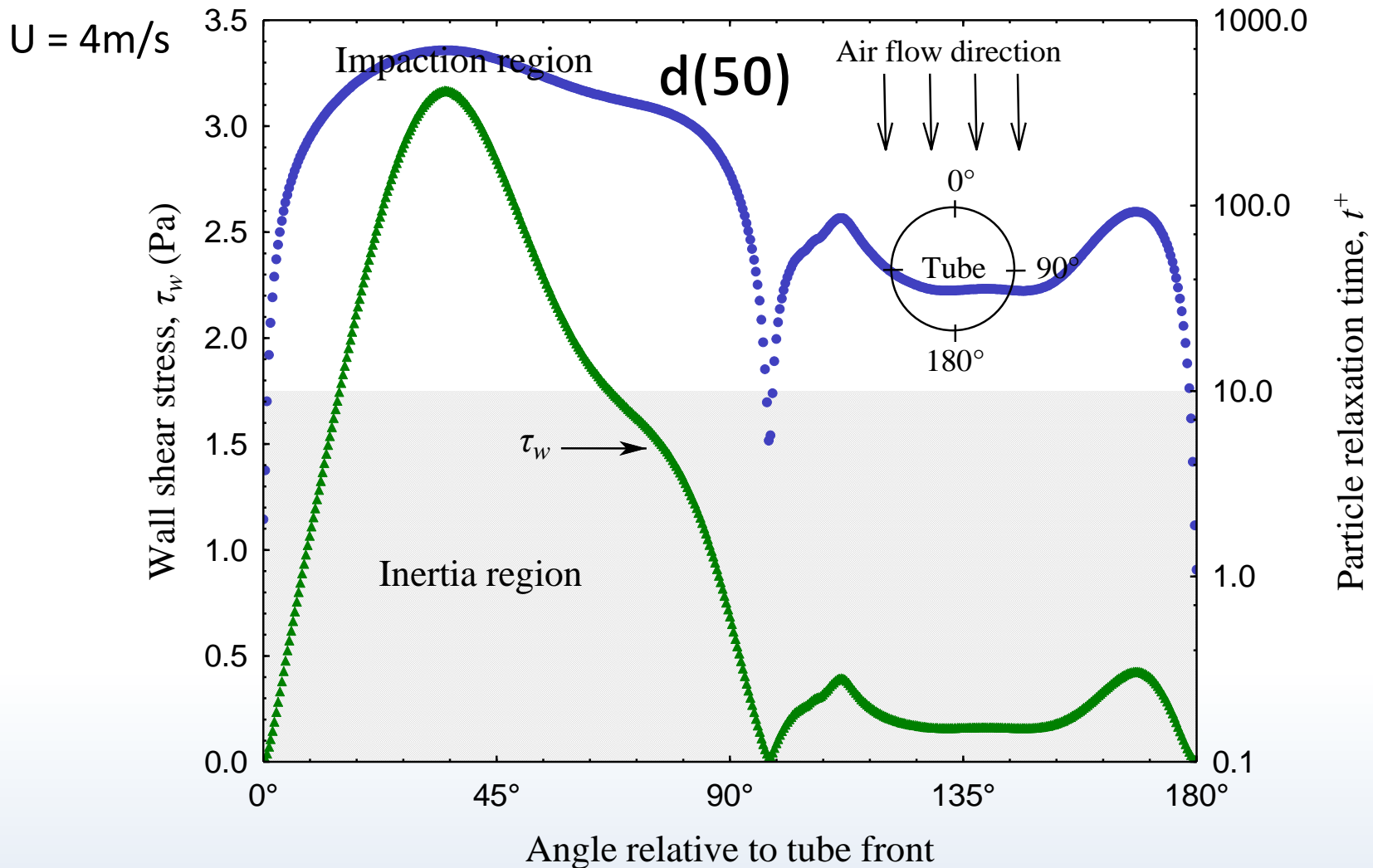
Wall Shear Stress and Deposition



Wall Shear Stress and Deposition



Wall Shear Stress and Deposition



Formulation of $j_{foul}(1/\tau_w)$

$$\frac{1}{h_{foul}} = \frac{1}{h_{clean}} + R_f \quad \text{where} \quad h_{clean} = \left(\frac{c_p \rho}{Pr^{2/3}} \frac{u_\infty}{\sigma} \right) j$$

$$\frac{1}{h_f} = \frac{1}{\left(\frac{c_p \rho}{Pr^{2/3}} \frac{u_\infty}{\sigma} \right) j} + \frac{A}{\tau_w}$$

Dependent on stickiness, Particle size, etc.

$$\frac{1}{j_f} = \frac{1}{j} + \left(\frac{c_p \rho}{Pr^{2/3}} \frac{u_\infty}{\sigma} \right) \frac{A}{\tau_w}$$

Since it varies around the tube, an average was taken

- Front facing
- Rear facing

What is the Best Shape?

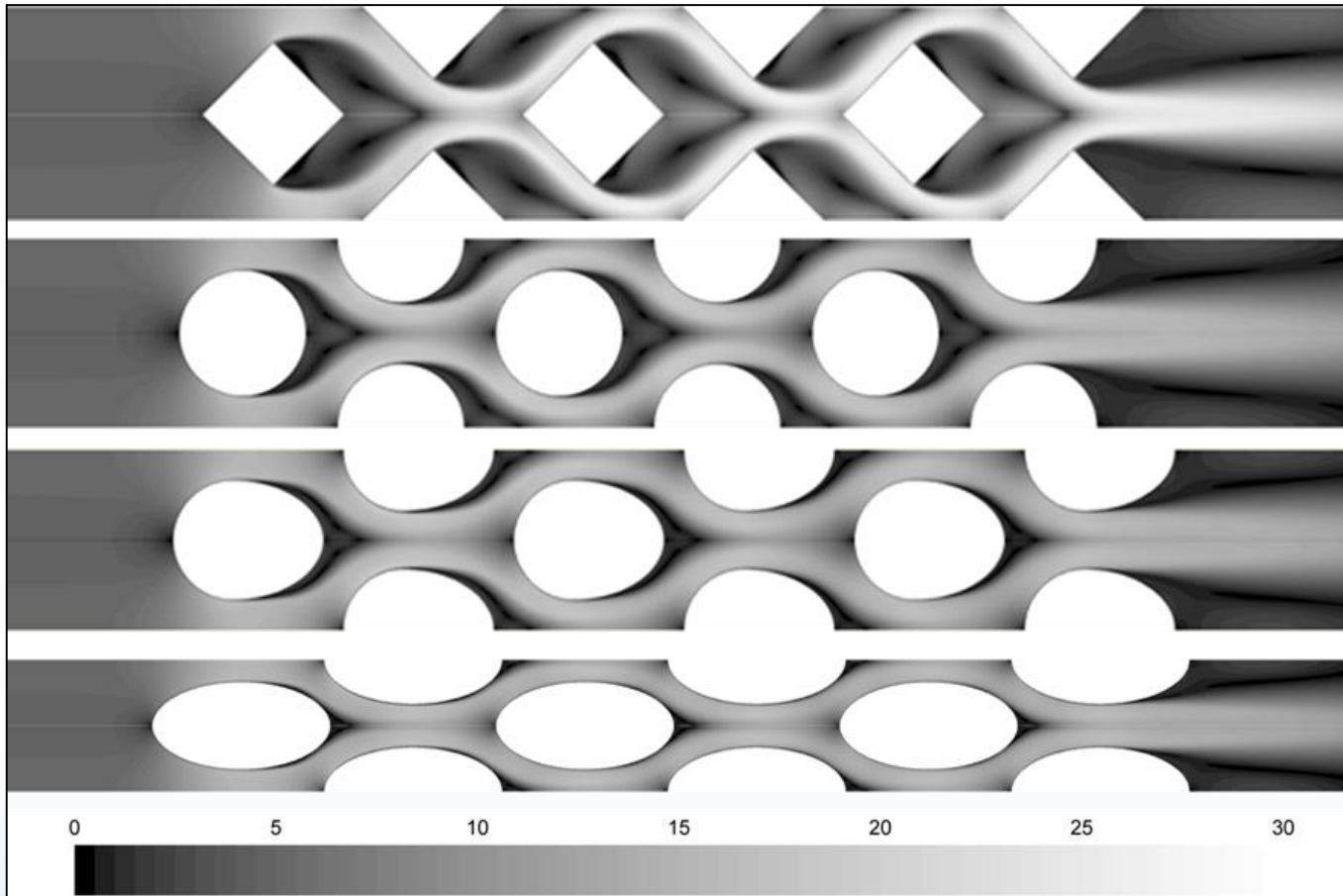
$$j_f / f^*$$

0.4

1.0

1.3

2.2

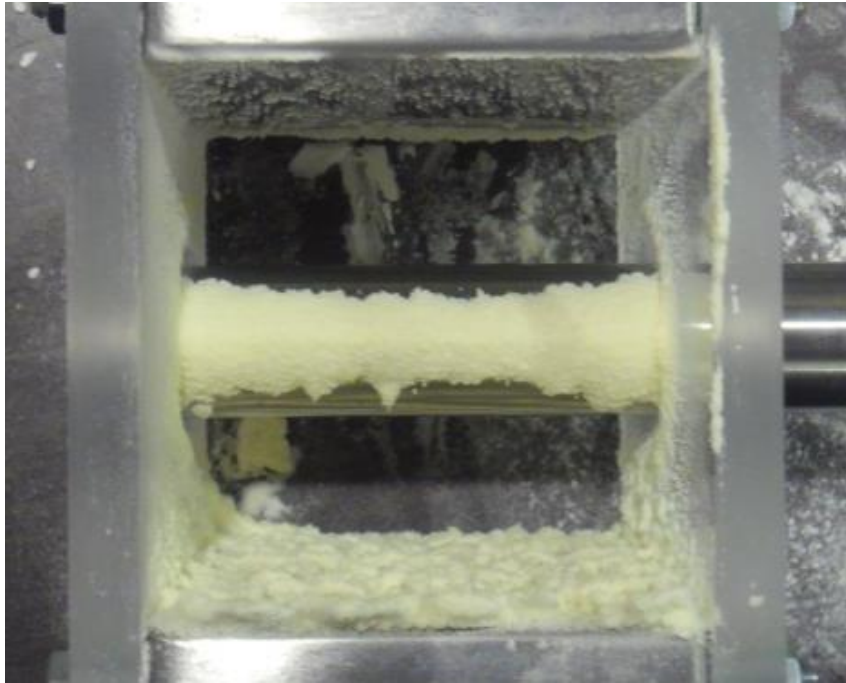


Round vs Elliptical

- On average, for the same Reynolds number
 - Round tube has 37% higher j_f
 - Ellipse has 65% reduction in f
 - So the better performing elliptical tube results from a very low pressure drop -> but larger volume HX
 - Ellipse is expected to have less fouling/deposition due to a smaller stagnation zone
- Limitation: the effect of fouling on the pressure drop has not been included -> experimental work

Preliminary Experimental Results

Round Tube



Elliptical Tube



Same air velocity, temperature and relative humidity

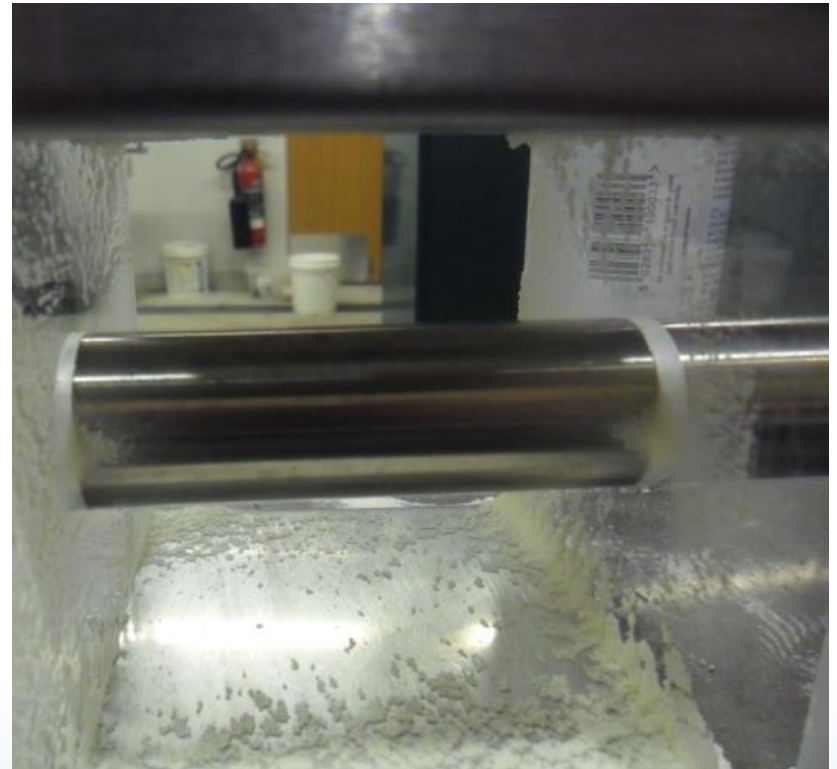
- Air temp / RH determine particulate surface stickiness
- Similar particle loading and time (equilibrium)

Round: Front vs Back

Front

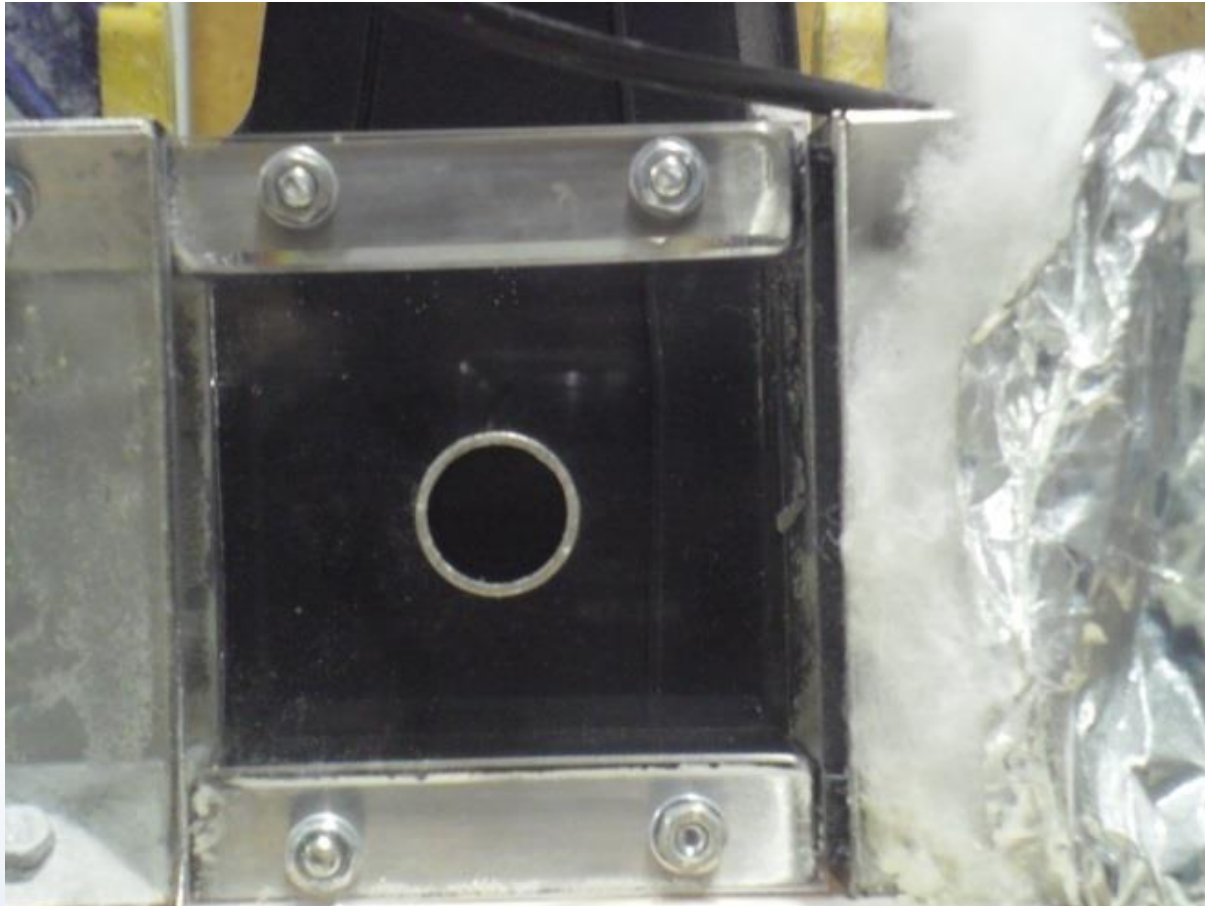


Back

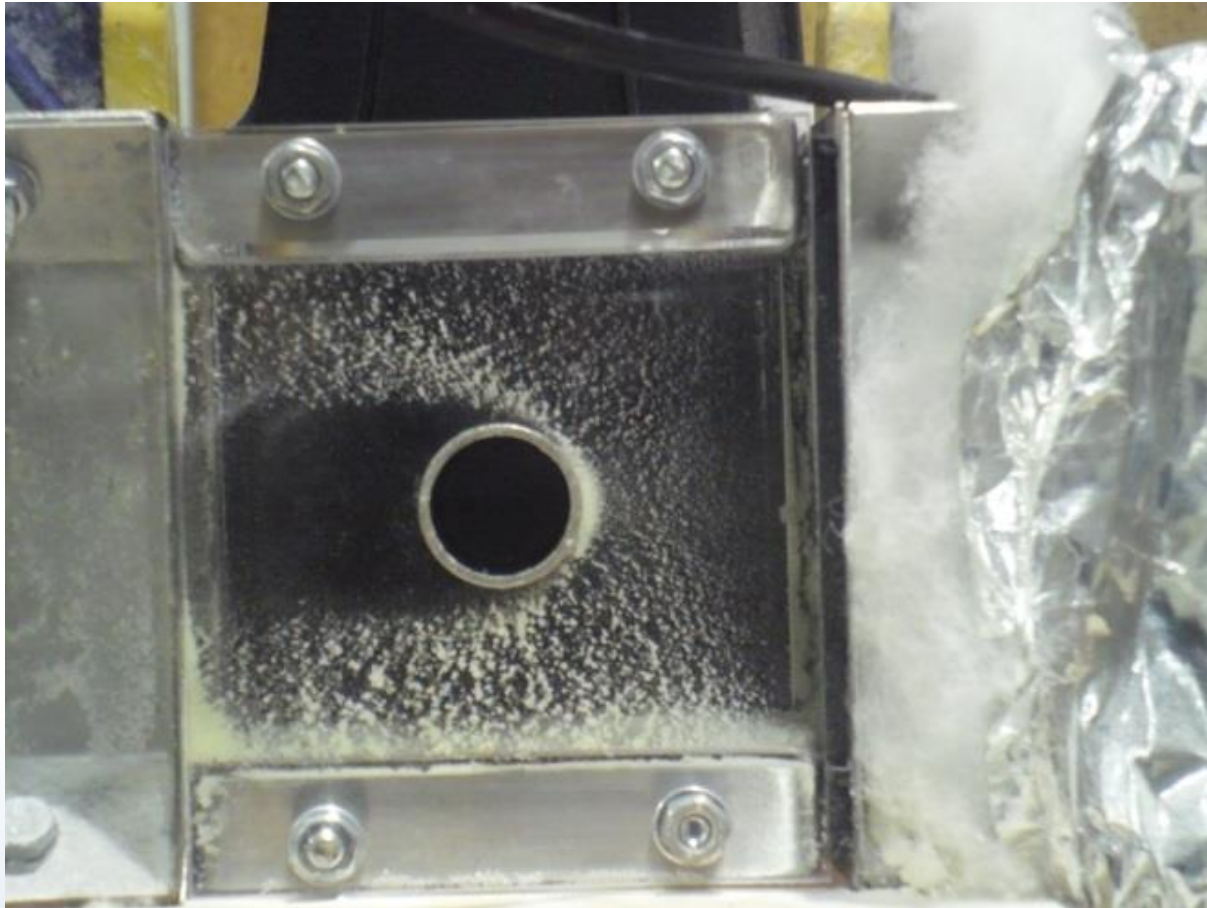


Testing in Fastforward

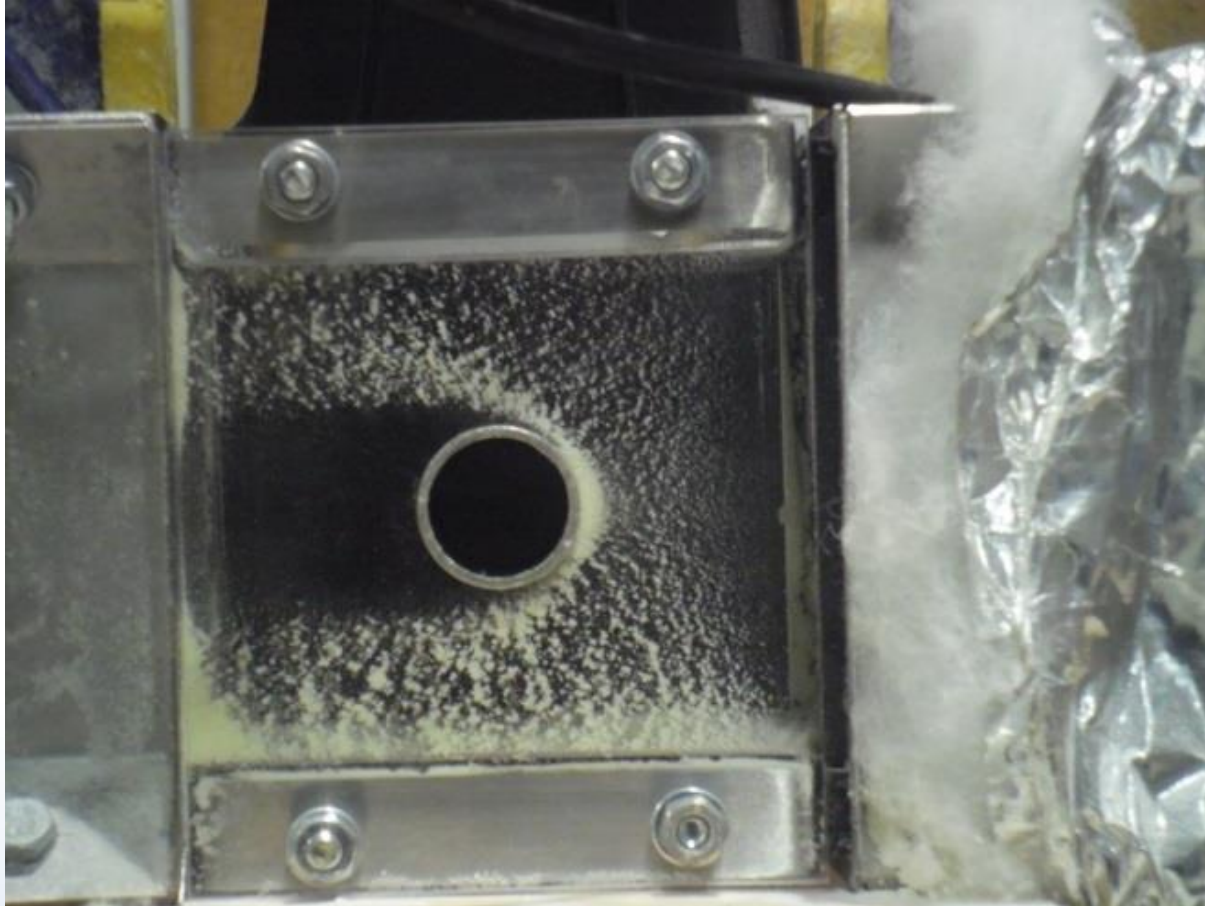
Start



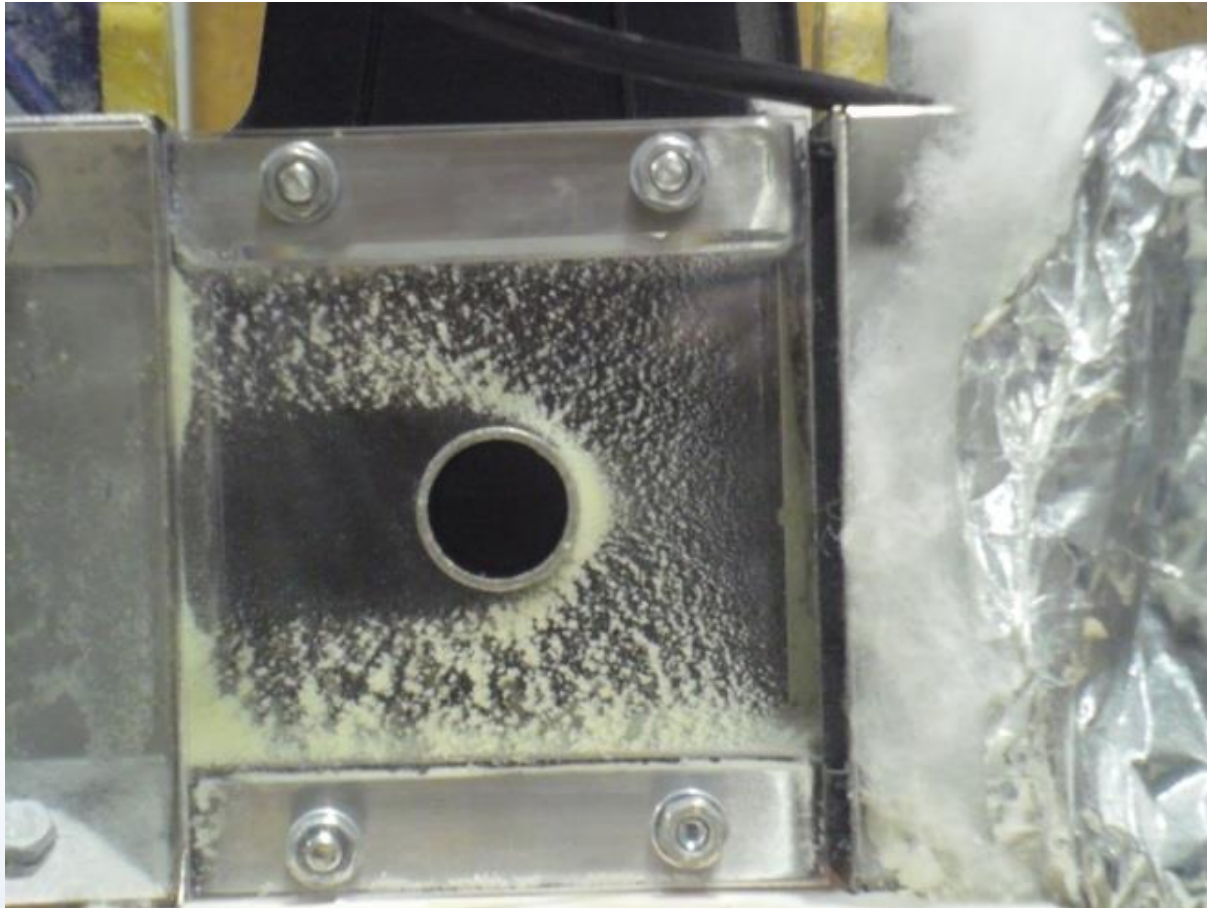
Testing in Fastforward 5 mins



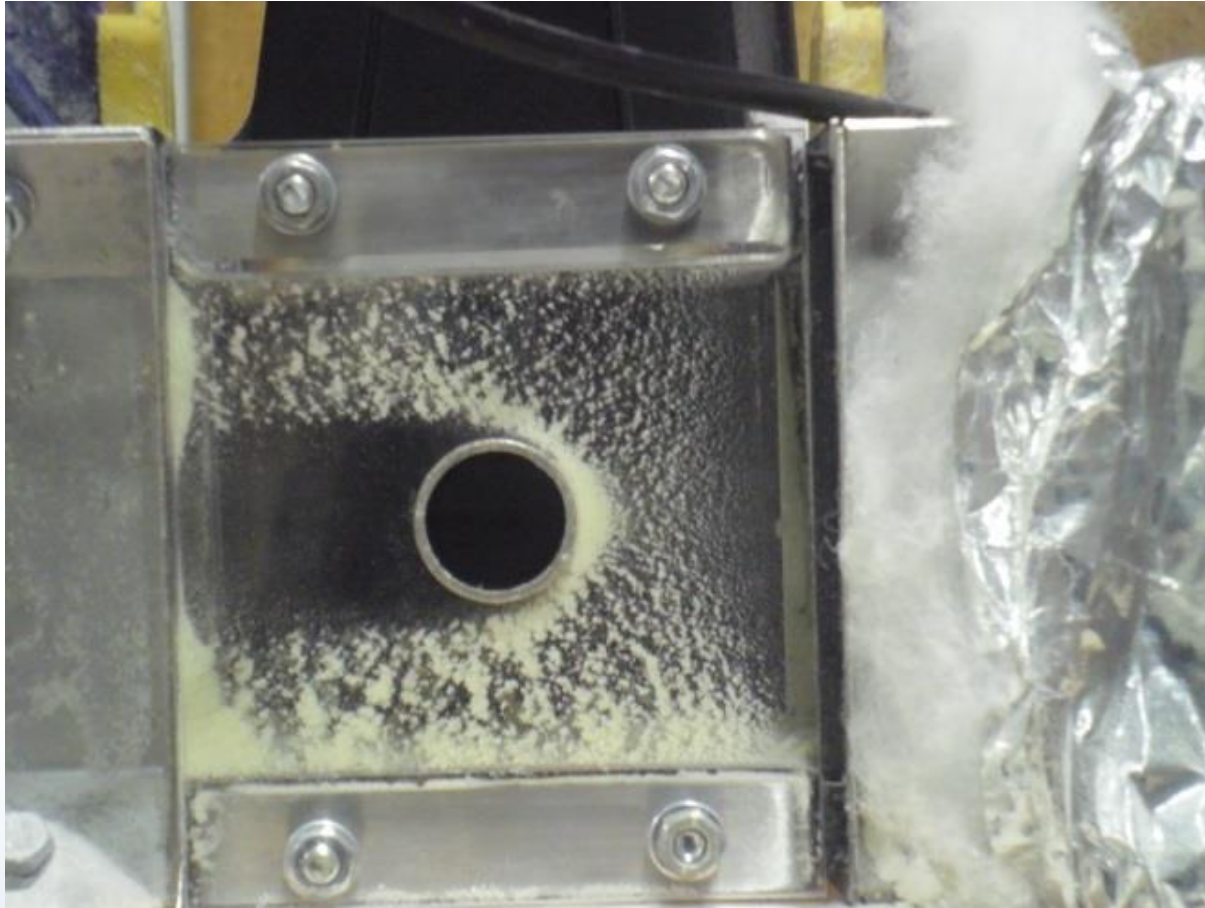
Testing in Fastforward 10 mins



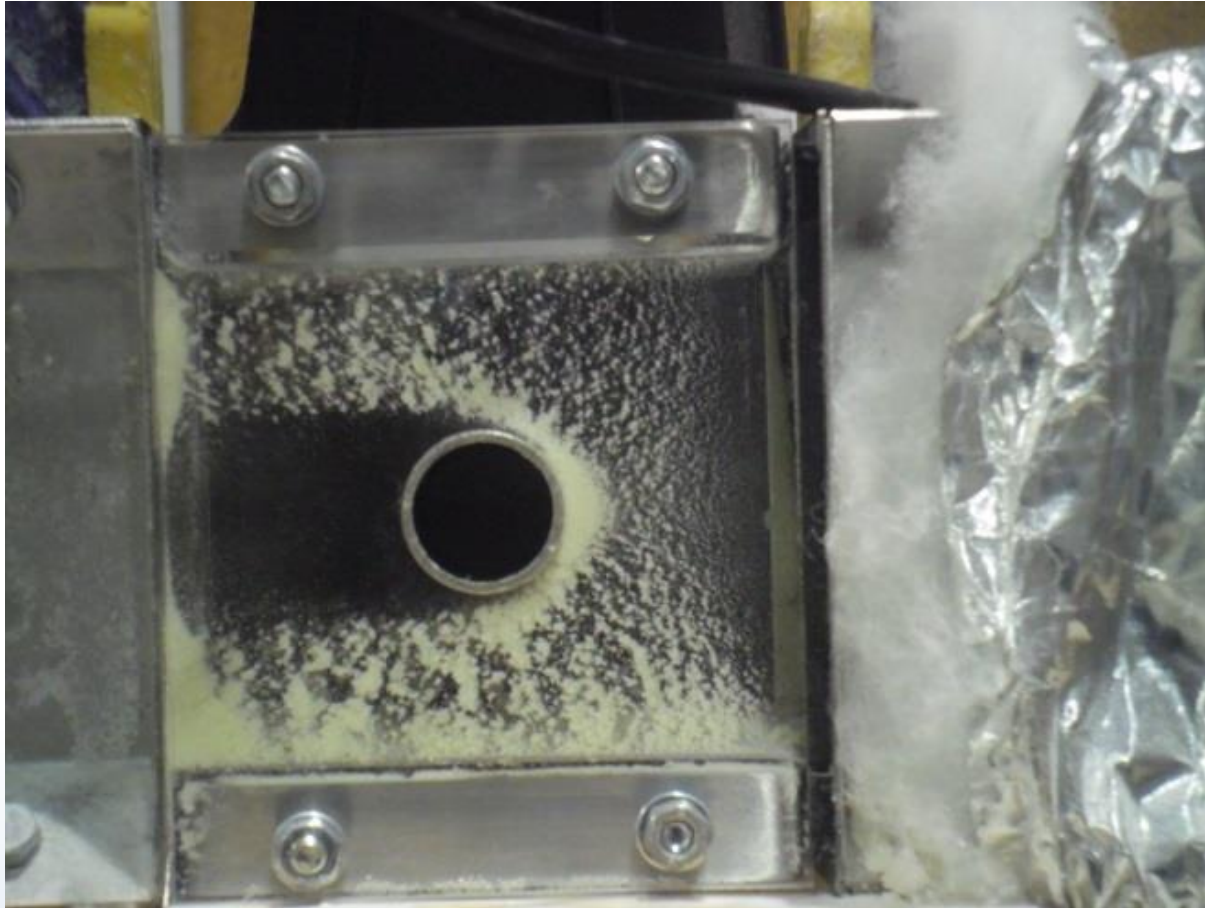
Testing in Fastforward 15 mins



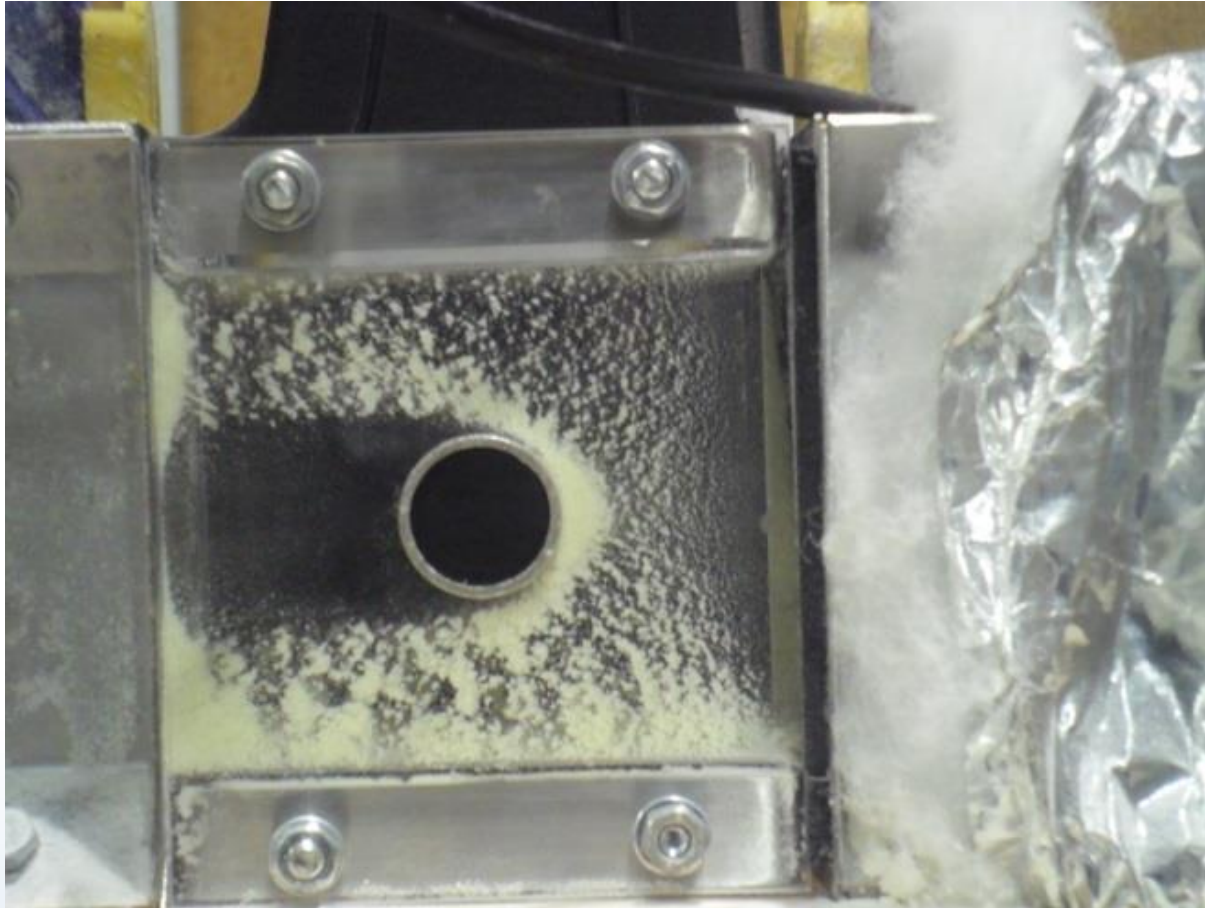
Testing in Fastforward 20 mins



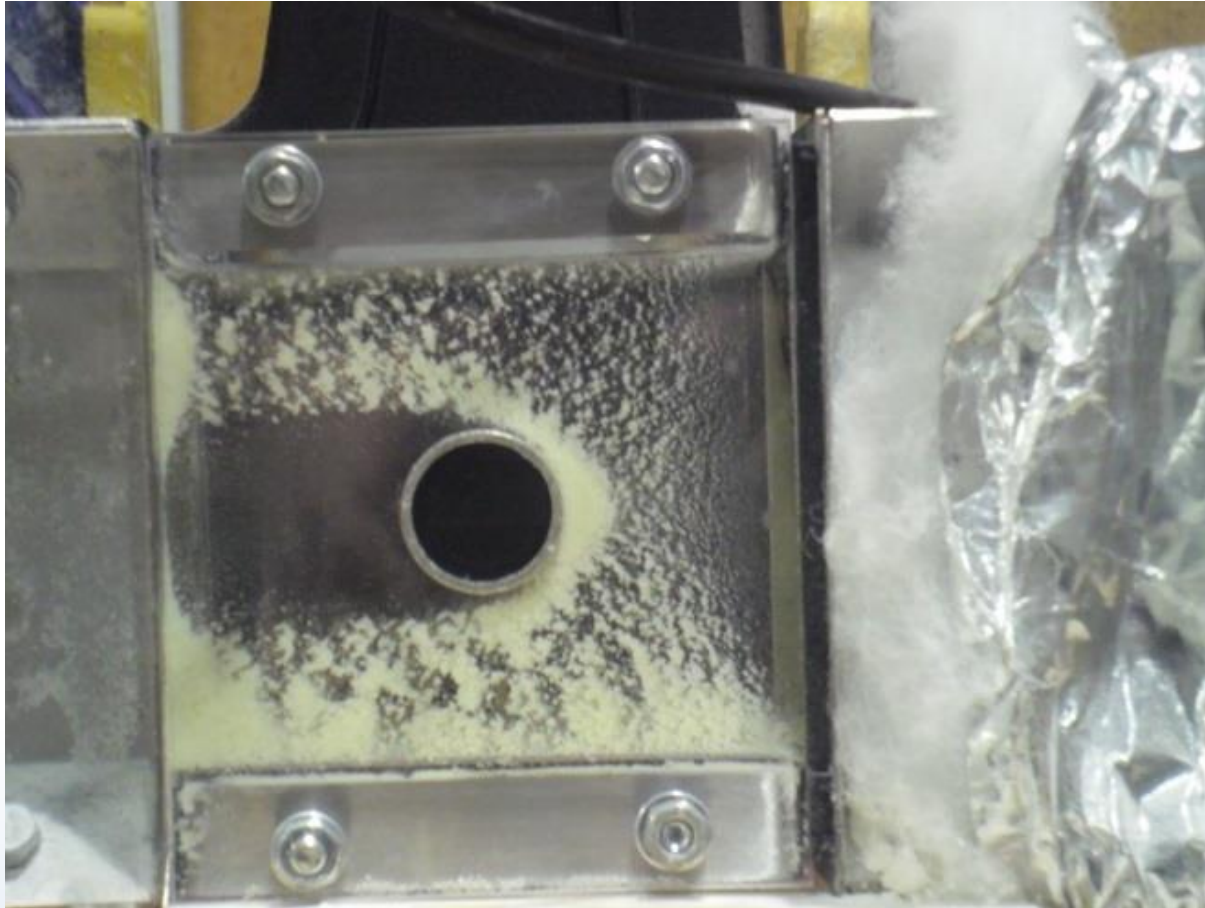
Testing in Fastforward 25 mins



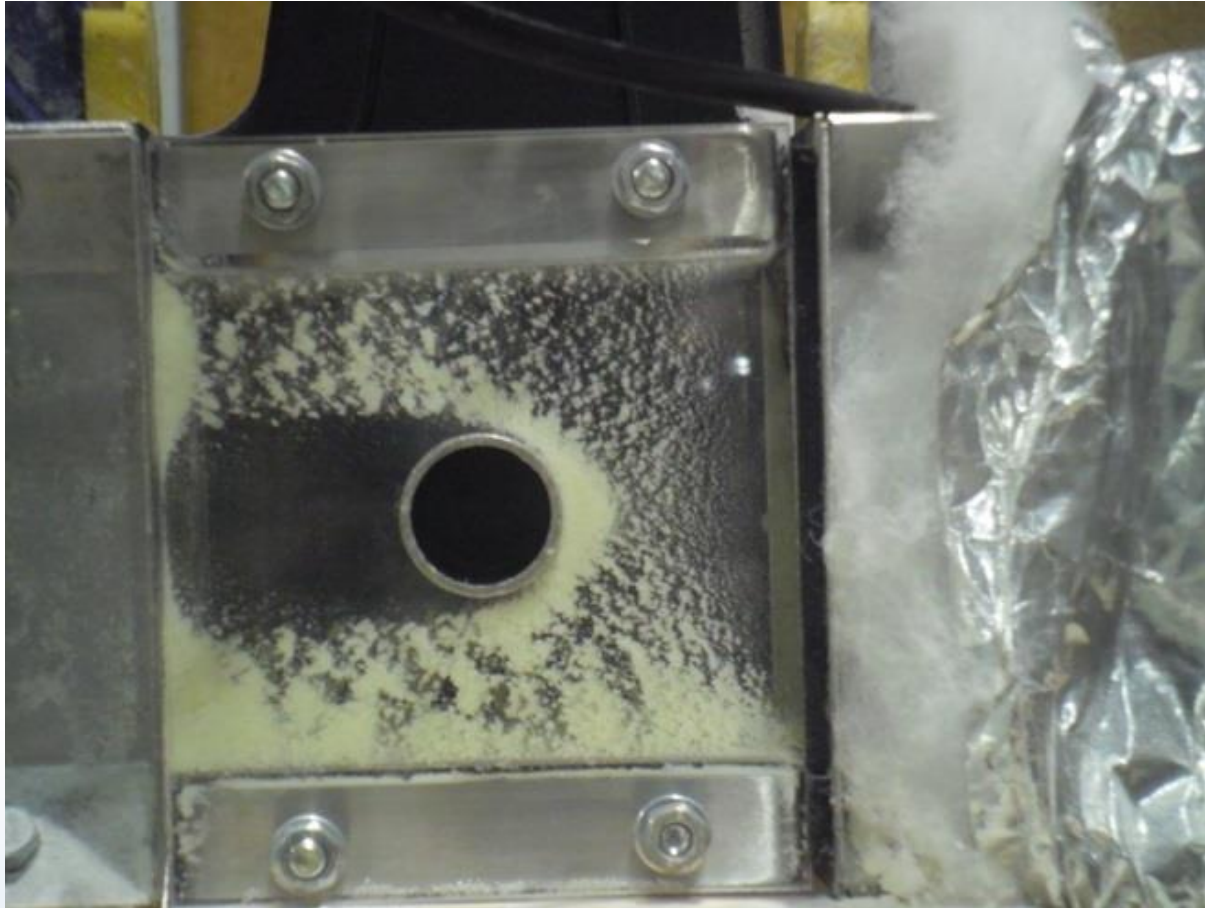
Testing in Fastforward 30 mins



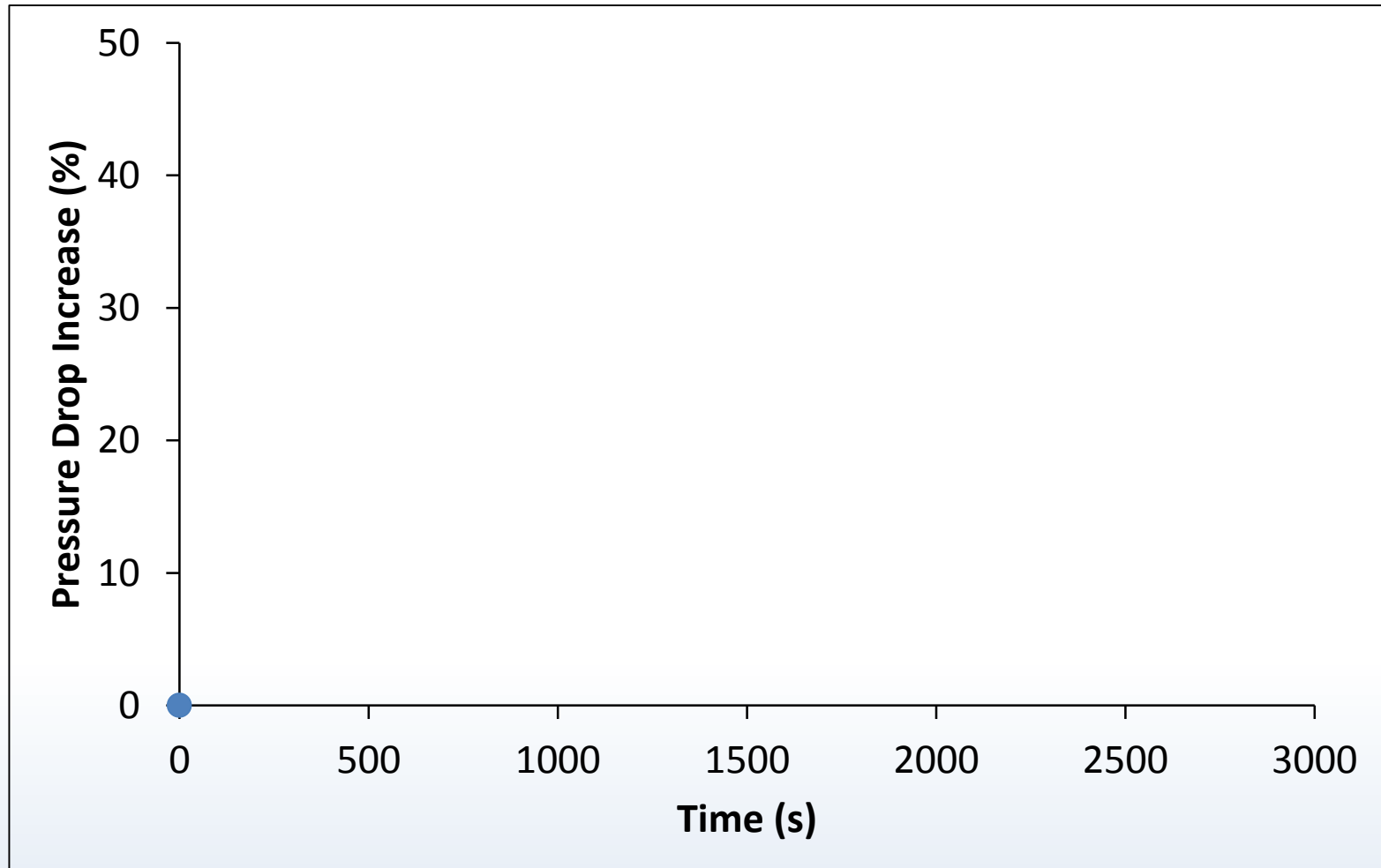
Testing in Fastforward 35 mins



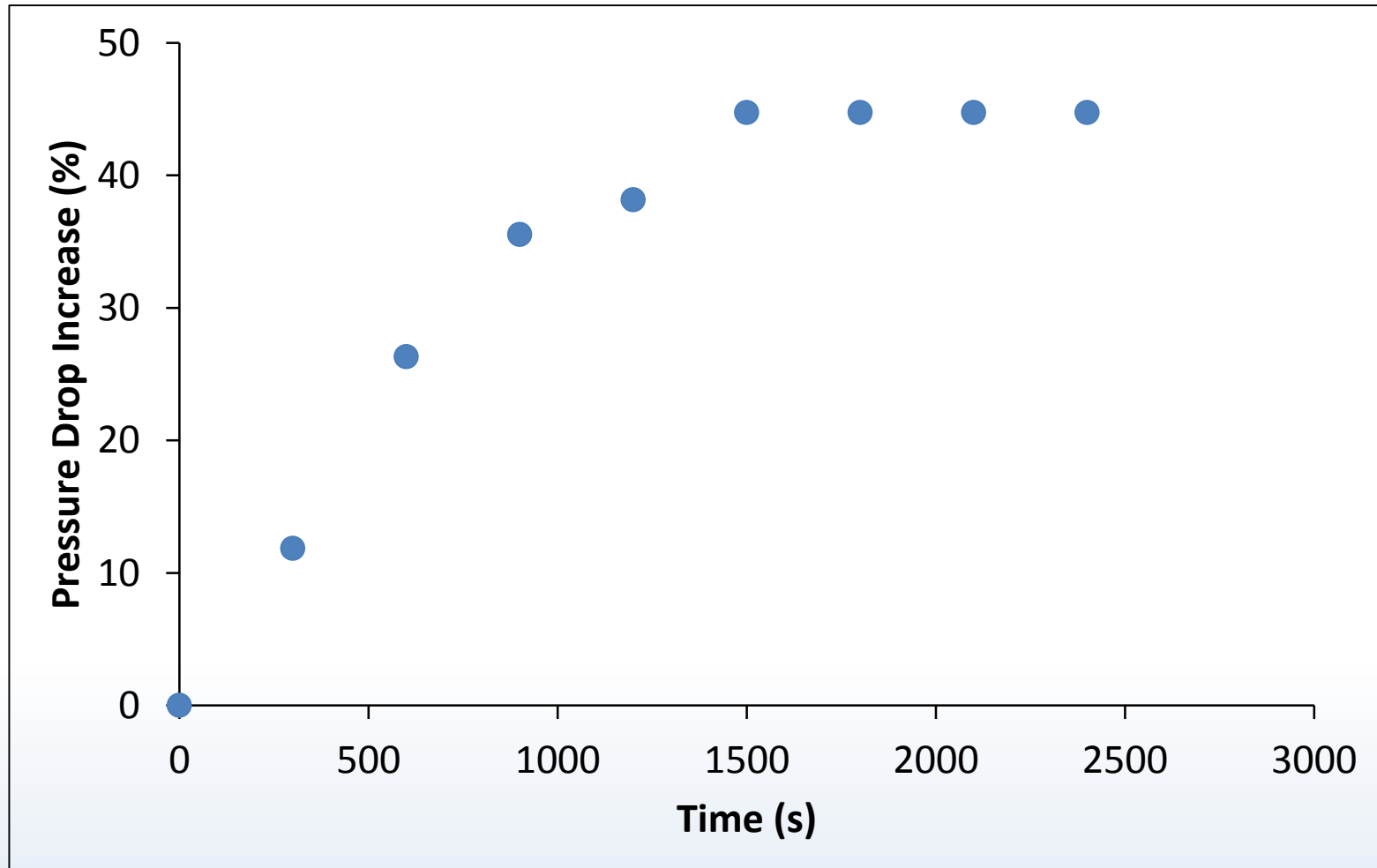
Testing in Fastforward 40 mins



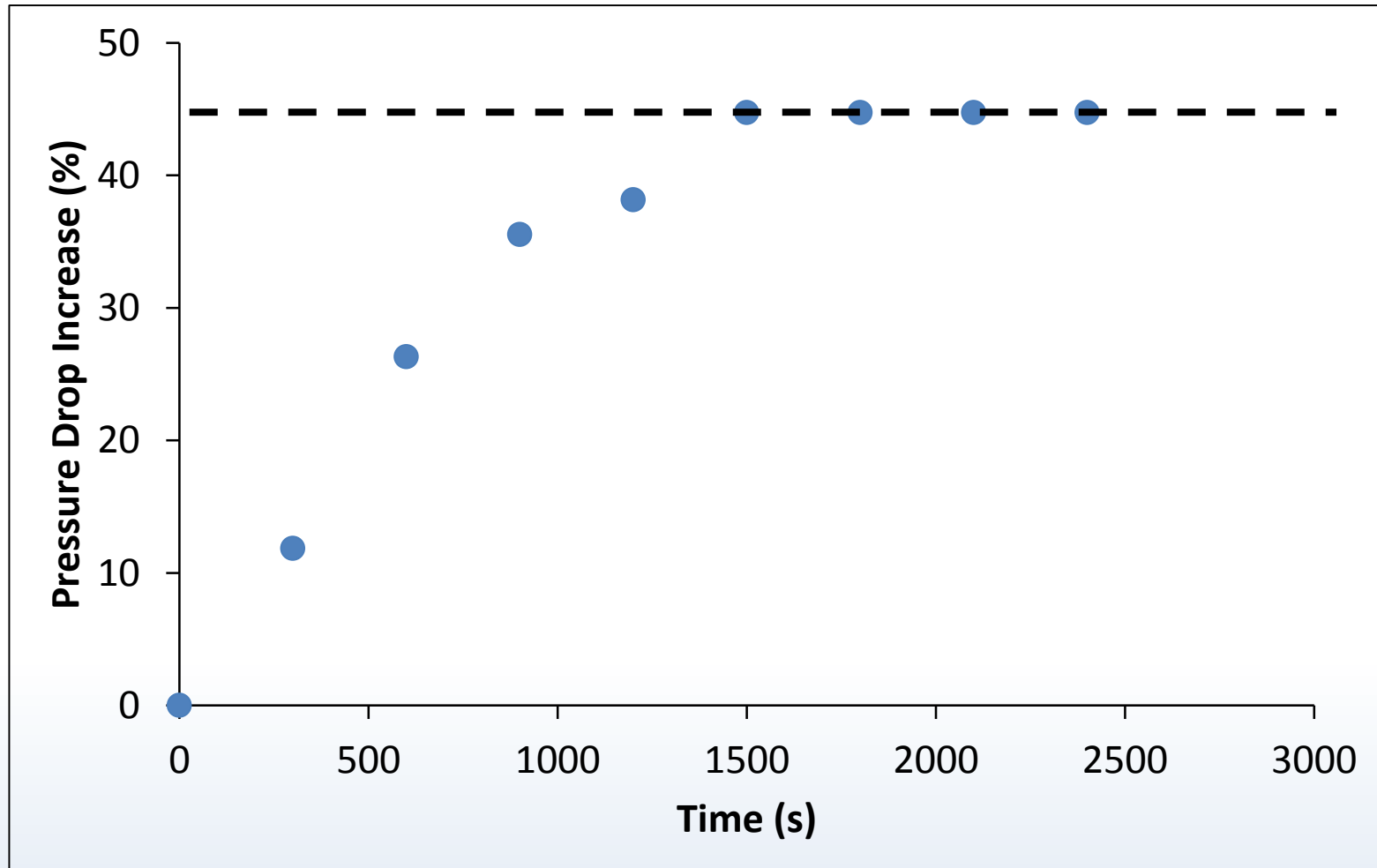
Pressure Drop Increase with Fouling



Pressure Drop Increase with Fouling



Pressure Drop Increase with Fouling



Summary

- Heat recovery from gas streams is important for high energy efficiency and it will be economic, one day
- Numerical results suggest elliptical tube can improve HX performance
- Preliminary experimental work adds to the understanding of how fouling affects the pressure drop
- Further considerations are needed in judging a best HX design, e.g. cost, availability

